



# AFRL

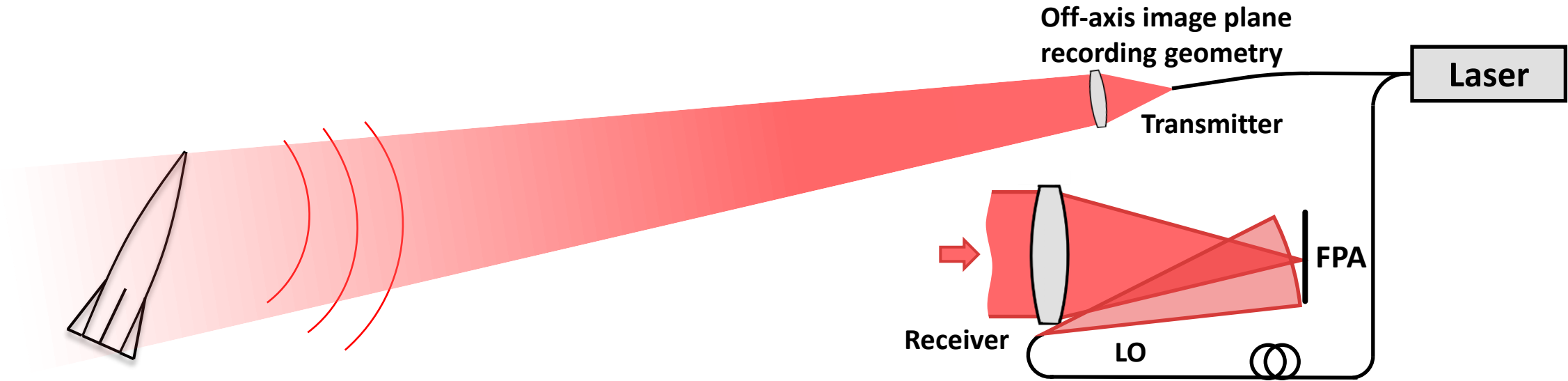
## Long range 3D imaging with digital holography

Matthias T. Banet

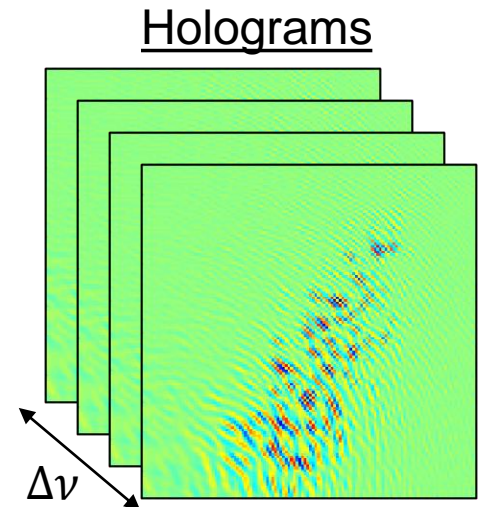
Directed Energy Directorate, Air Force Research Laboratory

[afrl.rdl.orgmailbox@us.af.mil](mailto:afrl.rdl.orgmailbox@us.af.mil)

# Digital holography with wavelength diversity enables 3D imaging



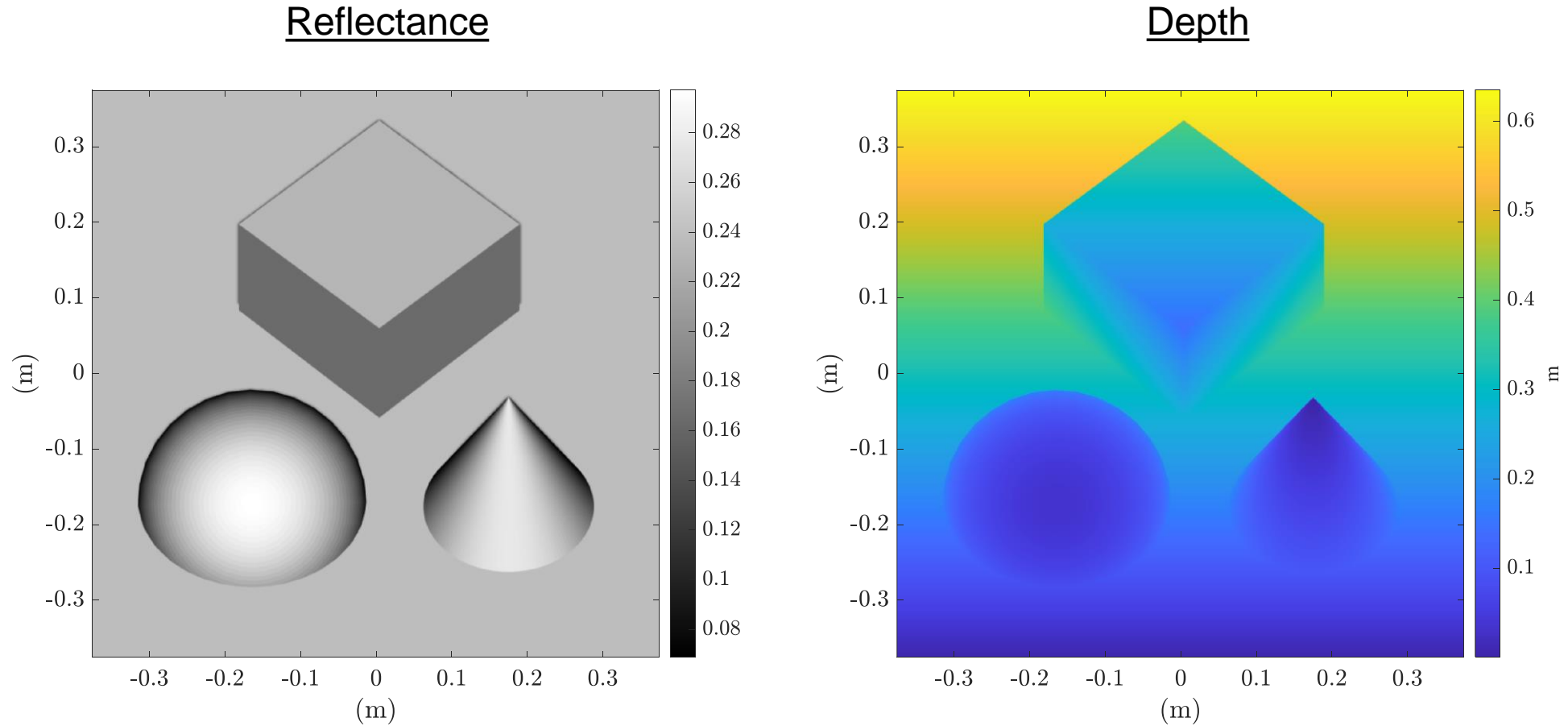
- Flood illuminate distant object with coherent light
- Interfere image of object with off-axis reference beam resulting in a hologram
- Repeat for many frequencies in a narrow bandwidth
- Perform Fourier transform over optical frequency to generate 3D image



Marron, J. C. and Schroeder, K. S., "Holographic laser radar," Opt. Lett. 18, 385–387 (Mar 1993).

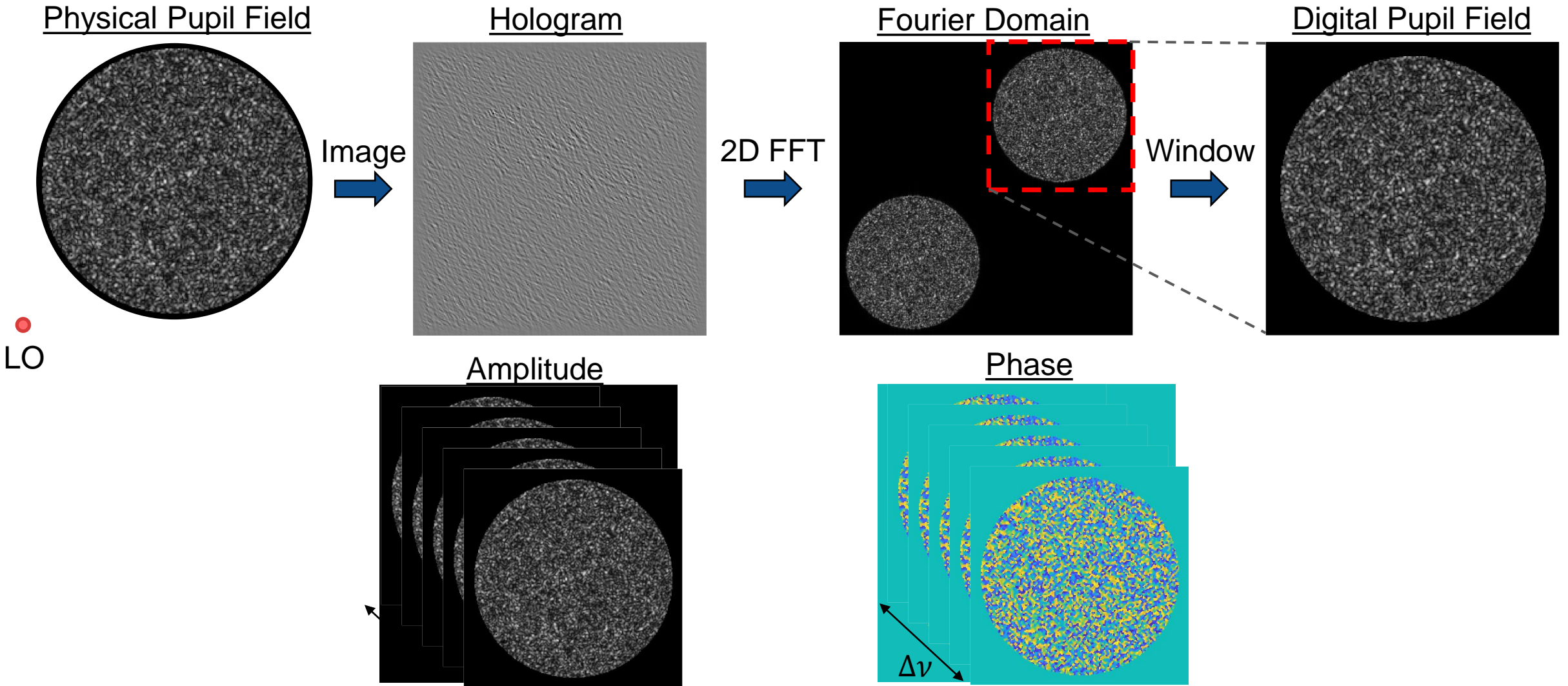


# Reflectance and depth profiles enable simulation of 3D imaging



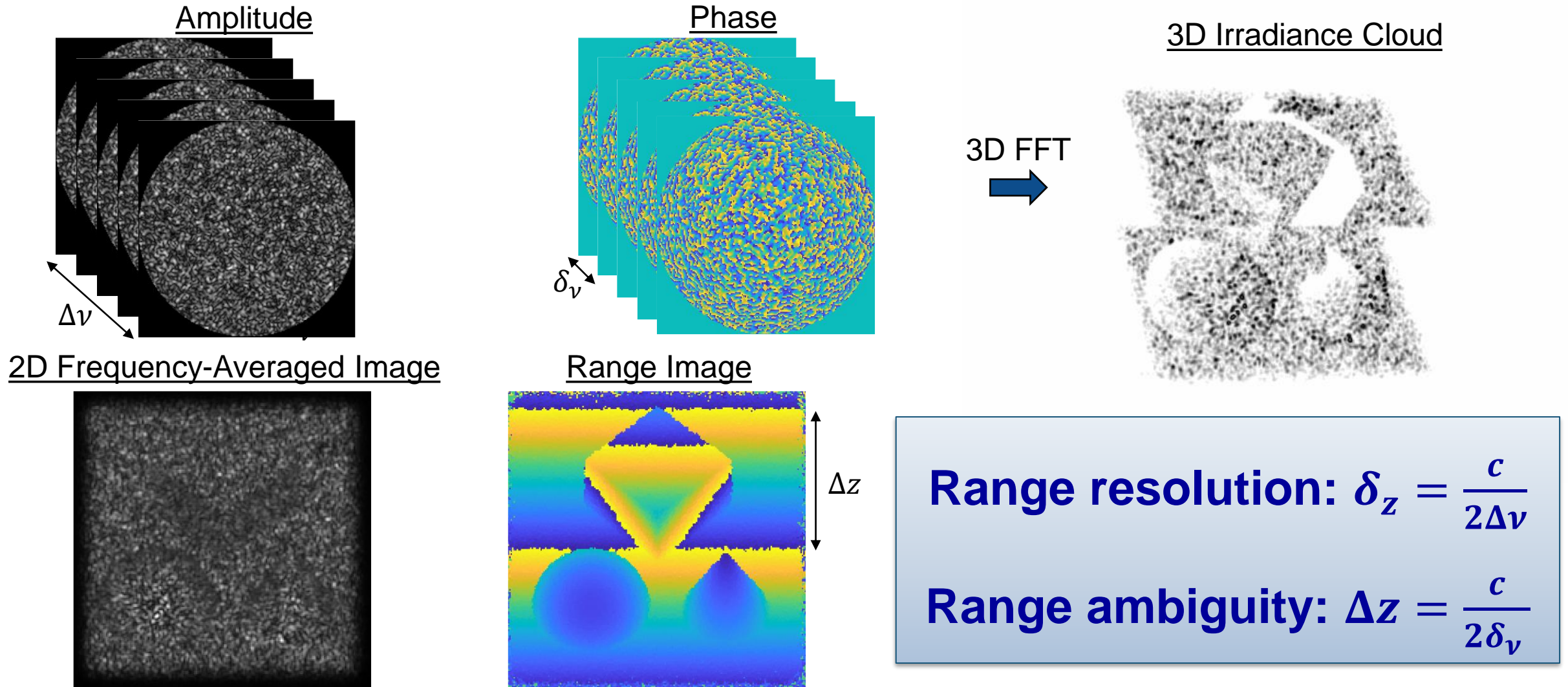
Blender Online Community, Blender - a 3D modelling and rendering package. Blender Foundation, Stichting Blender Foundation, Amsterdam (2018).

# Fourier processing provides amplitude and phase estimates

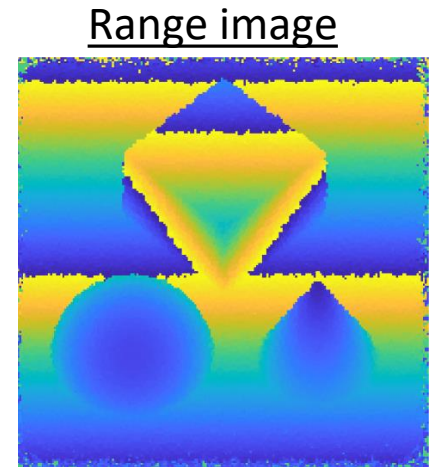
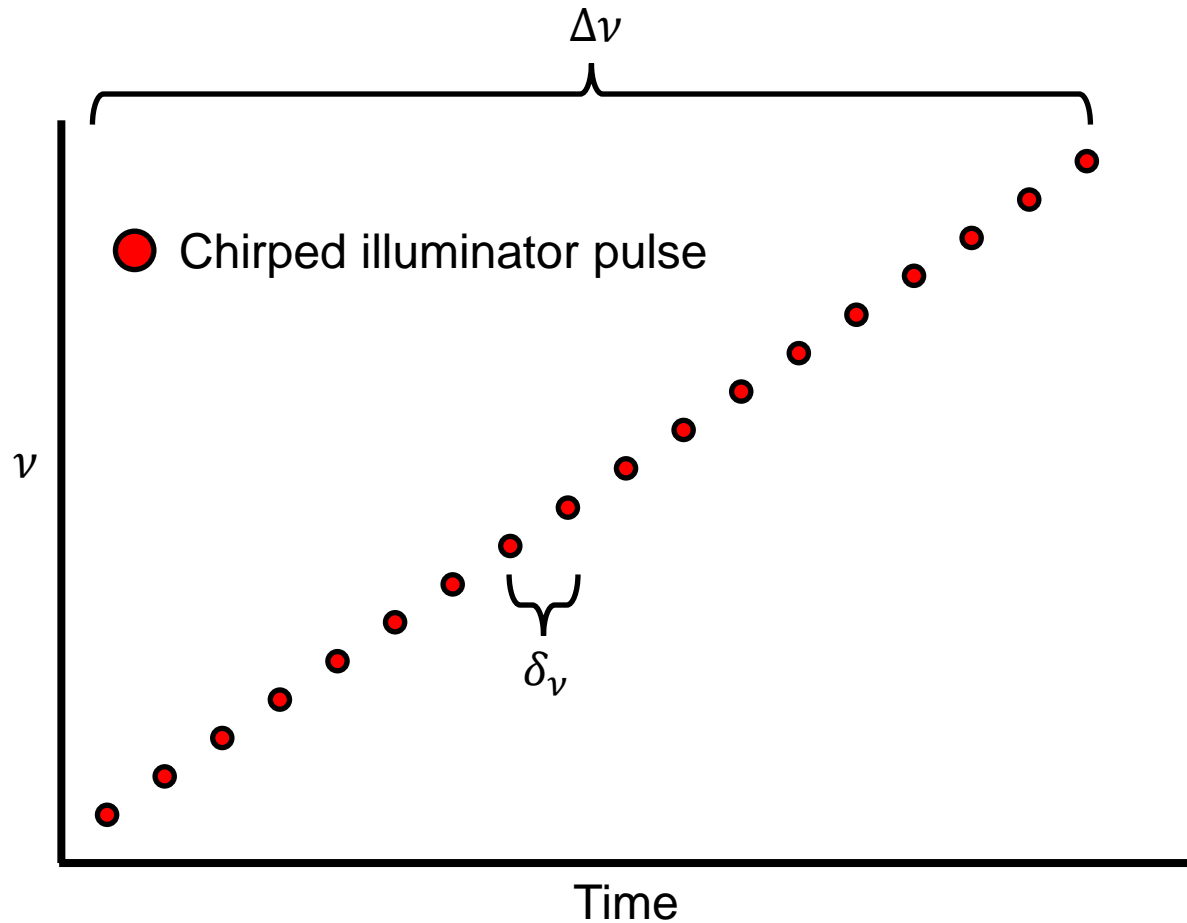


LO

# 3D and range imagery after Fourier transforming complex fields



# Conventional 3D imaging pulse train



Range image formed by taking z-location of maximum irradiance in 3D image

**Range resolution:**  $\delta_z = \frac{c}{2\Delta\nu}$

**Range ambiguity:**  $\Delta z = \frac{c}{2\delta\nu}$



# 3D imaging theory for rough, opaque objects

- Write object depth profile as

$$z_0 + Z(u, v)$$

- Write 2D coherent image of the object for some general illumination frequency,  $\nu$

$$U_i(u, v; \nu) = \exp(i4\pi\nu z_0/c) \times \underline{h(u, v)} * \{ \underline{U_{0,\perp}(u, v)} \exp[i4\pi\nu Z(u, v)/c] \}$$

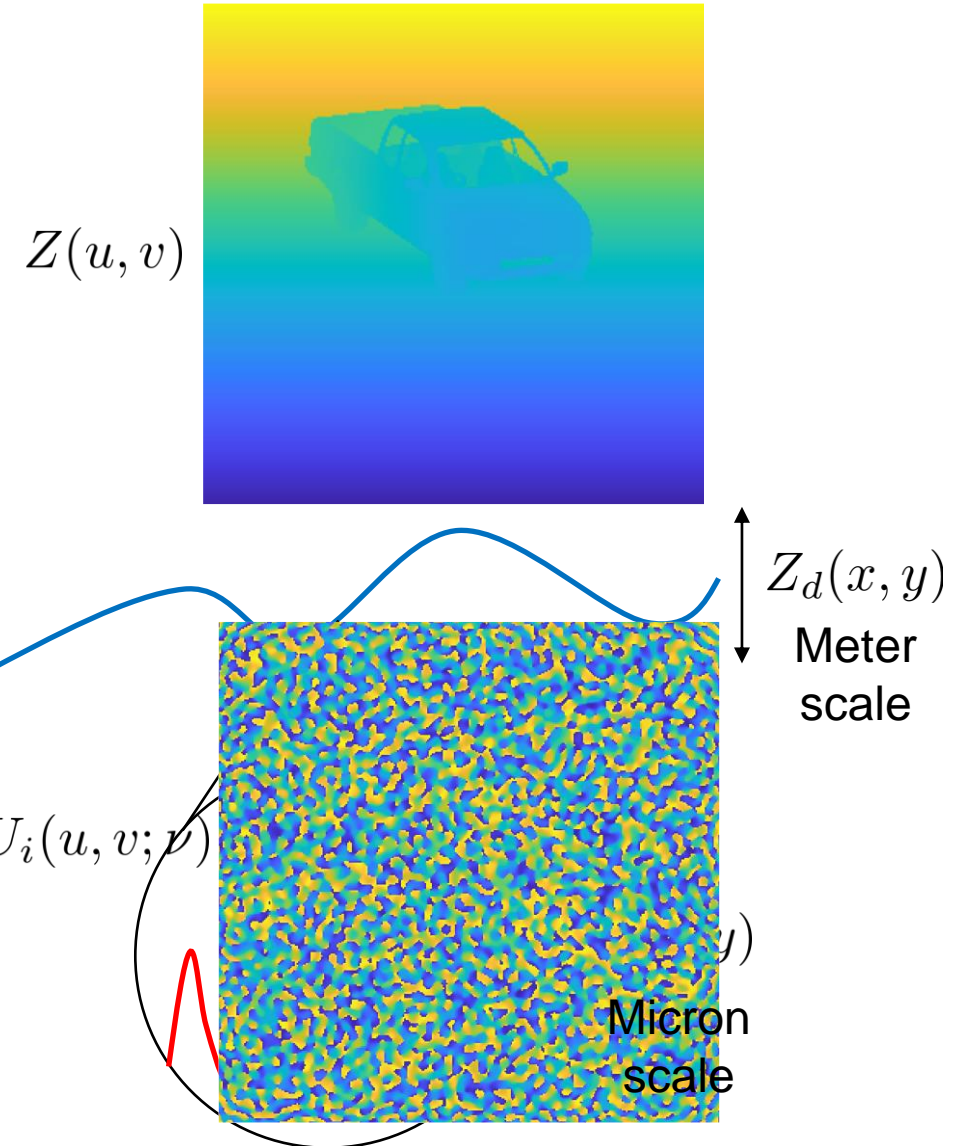
- Break up relative depth profile into coarse and rough components

$$Z(u, v) = \underline{Z_d(u, v)} + \underline{Z_r(u, v)}$$

- Rewrite 2D coherent image as

$$U_i(u, v; \nu) \approx \exp(i4\pi\nu z_0/c) \underline{\exp[i4\pi\nu Z_d(u, v)/c]} \times \underline{(h(u, v) * \{U_{0,\perp}(u, v) \exp[i4\pi\nu Z_r(u, v)/c]\})}$$

**Causes speckle!**





# 3D imaging theory for narrow illuminating bandwidths: $\delta_\nu/\nu_0 \sim 10^{-5}$

- If  $Z_r(u, v)$  is constant for a sequence of illumination frequencies,  $\nu_m$

$$U_i(u, v; \nu_m) \approx \exp(i4\pi\nu_m z_0/c) \exp[i4\pi\nu_m Z_d(u, v)/c] \times (h(u, v) * \{U_{0,\perp}(u, v) \exp[i4\pi\nu_m Z_r(u, v)/c]\})$$

- Write  $\nu_m$  as

$$\nu_m = \nu_0 + m\delta_\nu$$

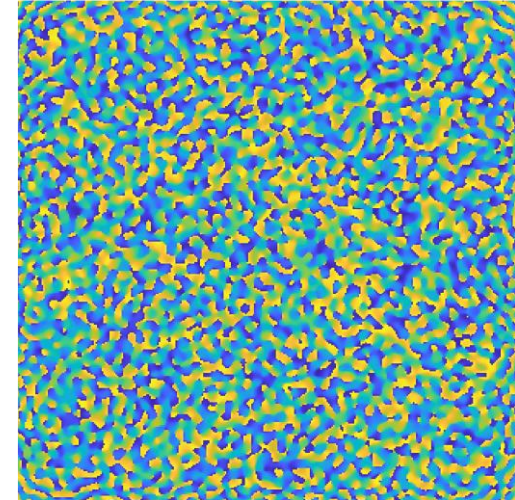
- Examine pertinent phasors containing  $\nu_m$

➡  $\exp[i4\pi(\nu_0 + m\delta_\nu)Z_d(u, v)/c]$

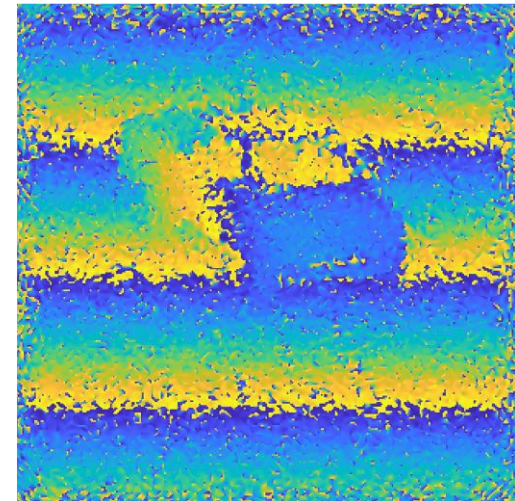
➡  $\exp[i4\pi(\nu_0 + m\delta_\nu)Z_r(u, v)/c] \approx \exp[i4\pi\nu_0 Z_r(u, v)/c]$

$$U_i(u, v; \nu_m) \approx \exp[i4\pi\nu_m z_0/c] \exp[i4\pi\nu_m Z_d(u, v)/c] \times (h(u, v) * \{U_{0,\perp}(u, v) \exp[i4\pi\nu_0 Z_r(u, v)/c]\})$$

$$\angle U_i(u, v; \nu_m)$$



$$\angle [U_i(u, v; \nu_1)U_i^*(u, v; \nu_2)]$$



Marron, J. C., et al. "Extended-range digital holographic imaging." *Laser Radar Technology and Applications XV*. Vol. 7684. SPIE, 2010.





# Assume that speckle phase is constant over frequency for small bandwidths

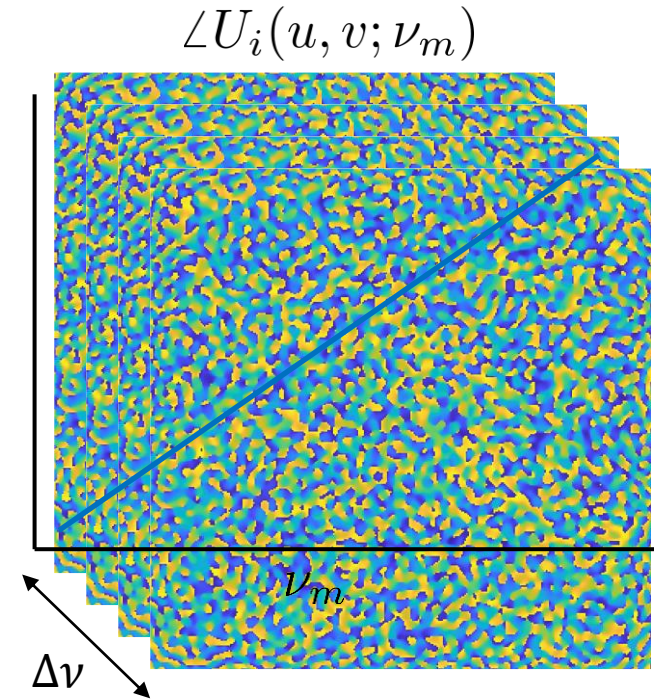
$$U_i(u, v; \nu_m) \approx \exp[i4\pi\nu_m z_0/c] \exp[i4\pi\nu_m Z_d(u, v)/c] \times (h(u, v) * \{U_{0,\perp}(u, v) \exp[i4\pi\nu_0 Z_r(u, v)/c]\})$$

- What happens when we Fourier transform  $U_i(u, v; \nu)$  over  $\nu_m$ ?

$$\mathcal{F}_{\nu_m} \{U_i(u, v; \nu_m)\} = \mathcal{A}(u, v) \mathcal{F}_{\nu_m} \{ \exp\{i4\pi\nu_m [z_0 + Z_d(u, v)]/c\} \} \Big|_{f_{\nu_m} = \frac{2z}{c}}$$

- Phase of  $\mathcal{A}(u, v)$  is “**speckle phase**” and is independent of  $\nu_m$
- Examine single transverse coordinate  $(u, v)$

**The coarse depth phase varies linearly with frequency for each transverse pixel**



Spoiler alert for later in the talk:  
Speckle phase can change with frequency due purely to *diffraction*

# Fourier transforming over frequency yields a 3D coherent image

$$\mathcal{F}_{\nu_m} \{U_i(u, v; \nu_m)\} =$$

$$\underline{A(u, v)} \mathcal{F}_{\nu_m} \{ \exp\{i4\pi\nu_m [z_0 + Z_d(u, v)]/c\} \} \Big|_{f\nu_m = \frac{2z}{c}}$$

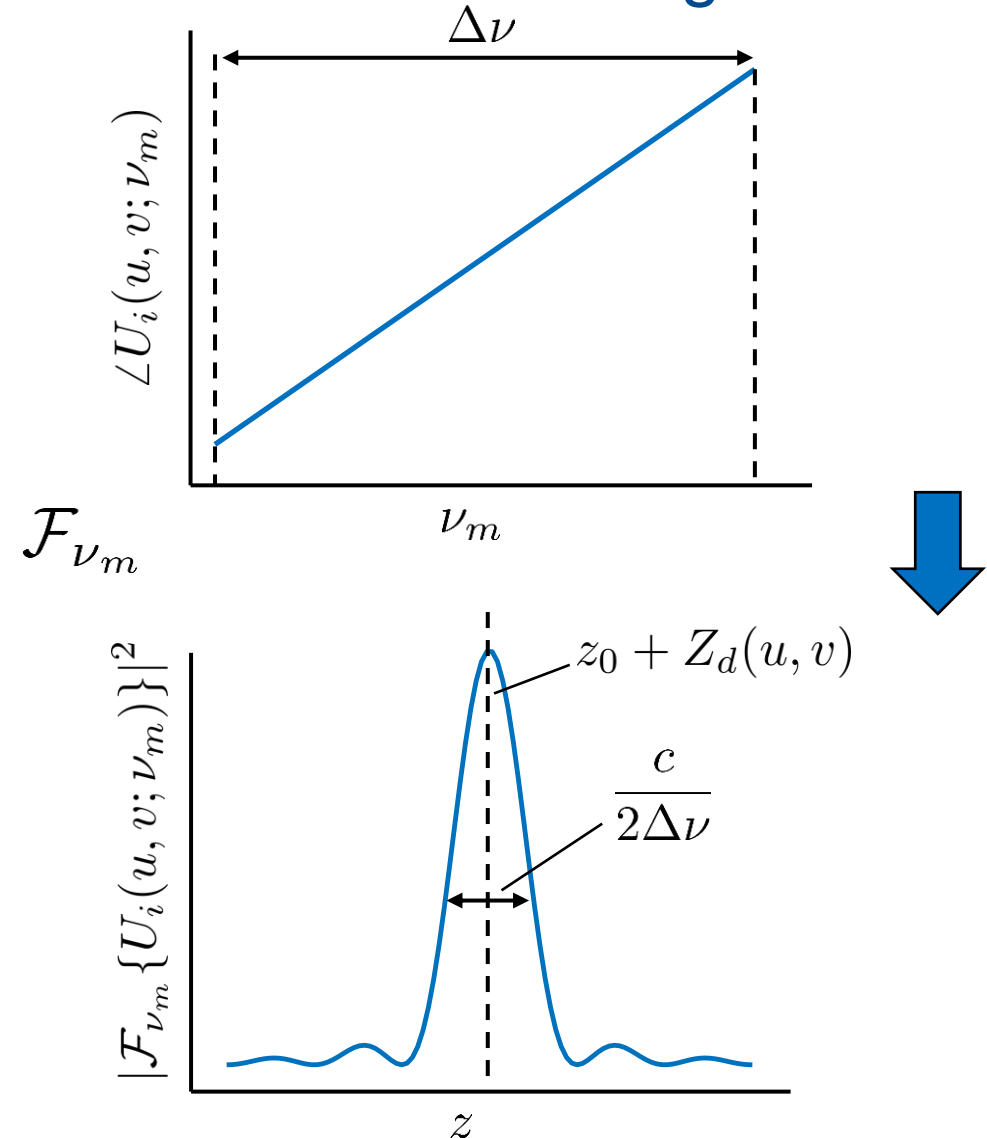
- Use the Fourier shift theorem to write

$$\mathcal{F}_{\nu_m} \{U_i(u, v; \nu_m)\} \propto$$

$$\underline{A(u, v)} \mathcal{F}_{\nu_m} \{B(\nu_m)\} * \underline{\delta\{z - [z_0 + Z_d(u, v)]\}}$$

- $B(\nu_m)$  is the optical frequency spectrum with width  $\Delta\nu$
- $\mathcal{F}_{\nu_m} \{B(\nu_m)\}$  determines range resolution:  $c/(2\Delta\nu)$

**Fourier transforming over frequency grants access to the object depth profile**



# What happens when speckle phase changes pulse to pulse?

- Underlying object reflectance for illumination frequency,  $\nu$ :

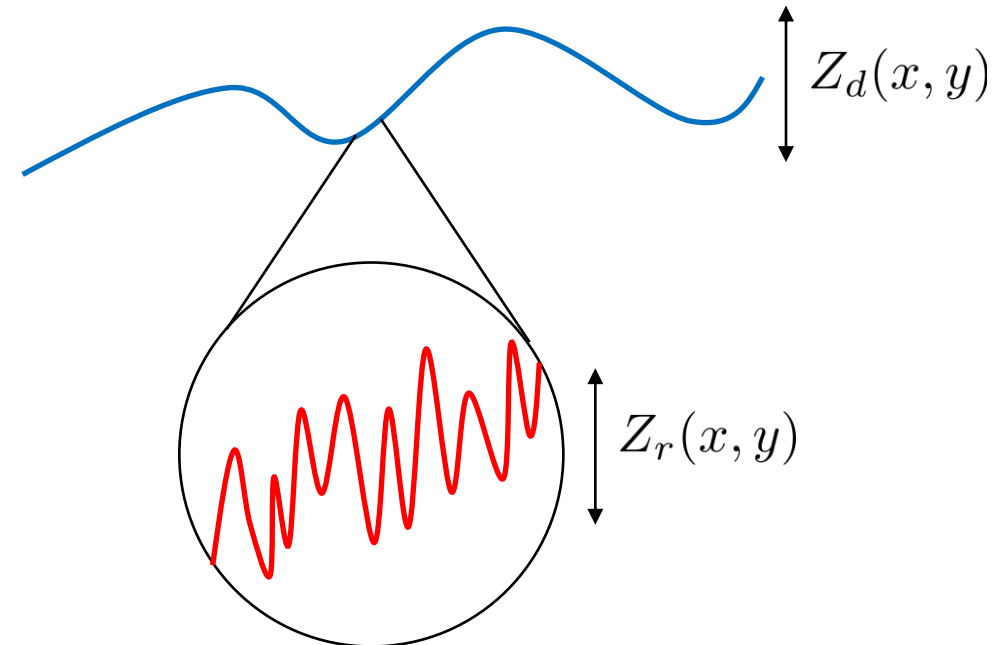
$$A(\xi, \eta) \exp[i\phi(\xi, \eta)]$$

$$\phi(\xi, \eta) = \frac{4\pi\nu}{c} [z_0 + \underline{Z_d(\xi, \eta)} + \underline{Z_r(\xi, \eta)}]$$

$$\phi_r(\xi, \eta) = \frac{4\pi\nu}{c} Z_r(\xi, \eta)$$

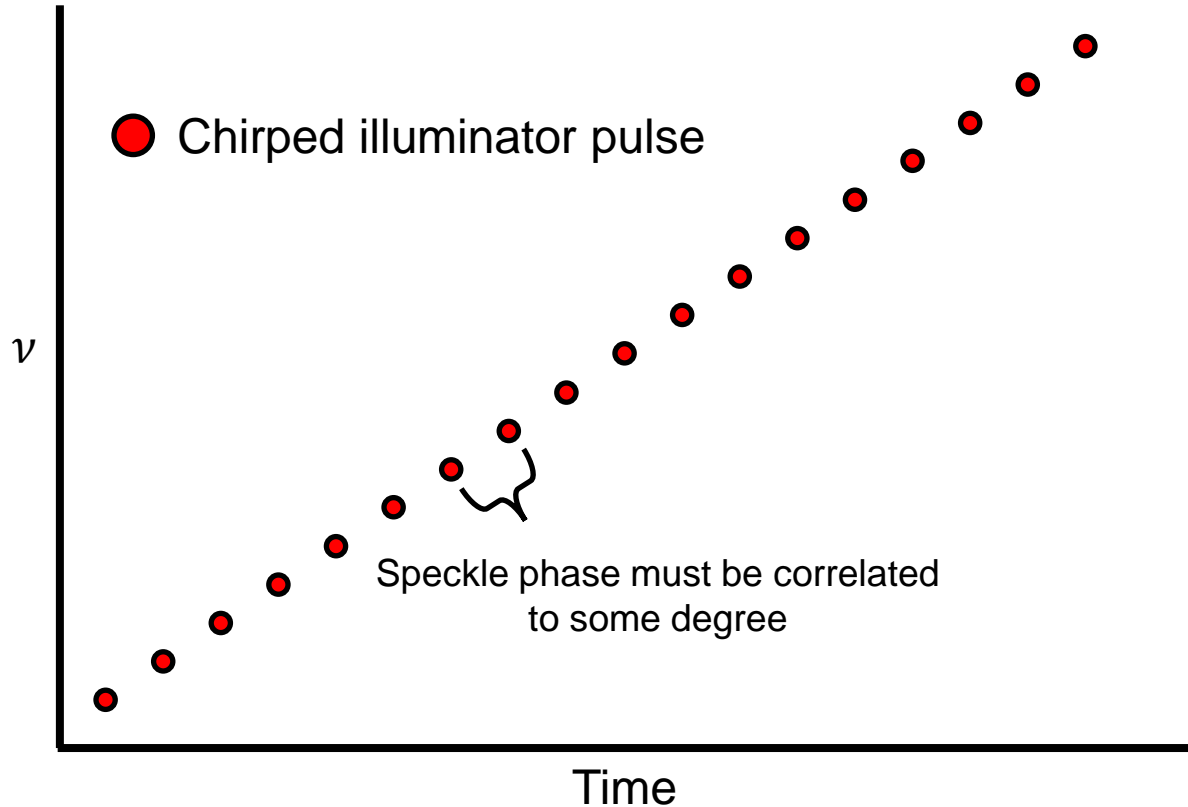
- We are assuming that  $\phi_r$  does not change for small changes in  $\nu$ , but it can still change when  $Z_r$  changes!

**Speckle phase in the image plane must have some degree of correlation pulse-to-pulse in order to form a range image**





# Conventional 3D imaging: what if the surface roughness profile changes over time?

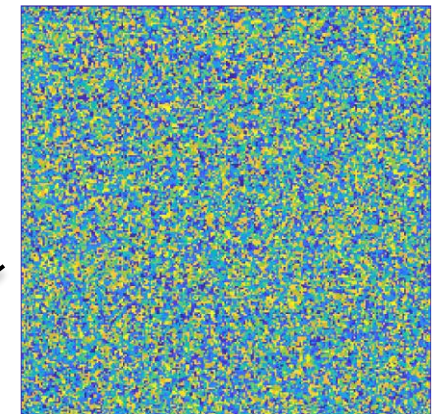
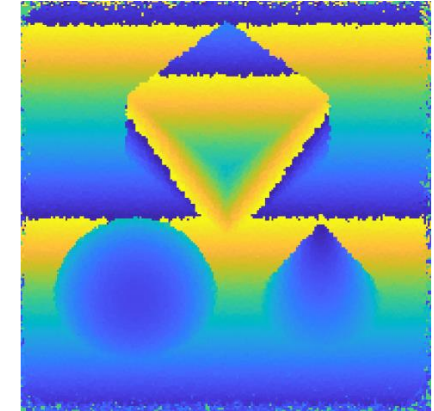


Common or correlated speckle phase pulse-to-pulse

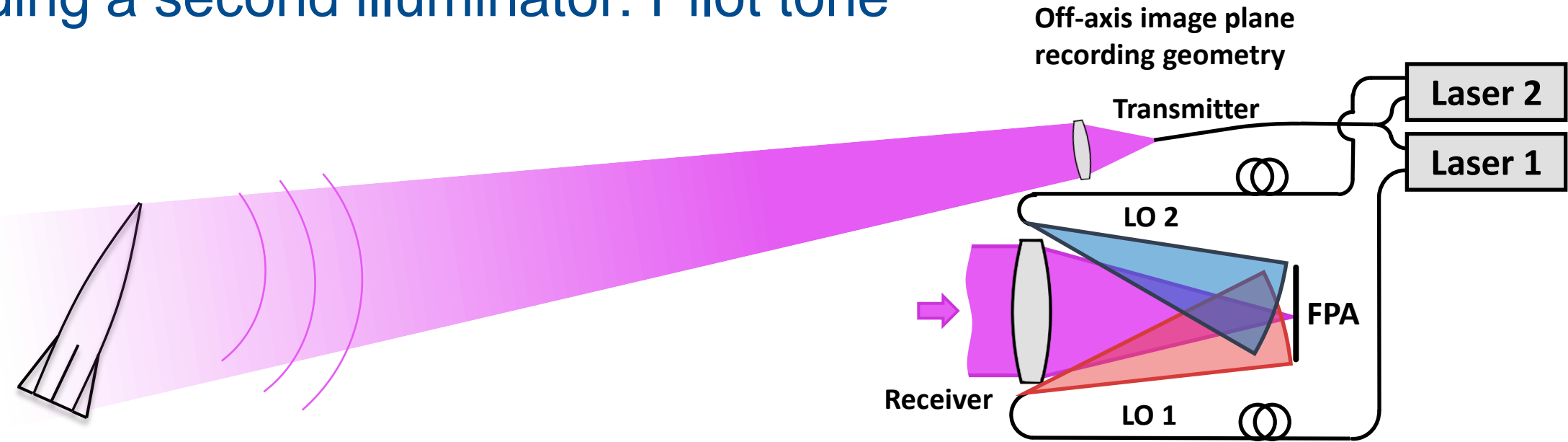
Independent speckle phase pulse-to-pulse

Can occur when object is moving/vibrating over image collection

Range images



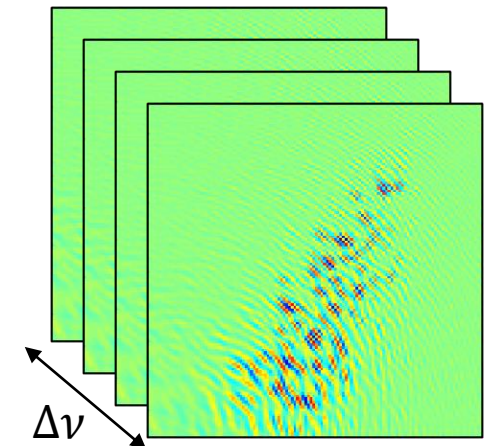
# Adding a second illuminator: Pilot tone



■ = pilot tone    
 ■ = chirped illuminator    
 ■ = both sources

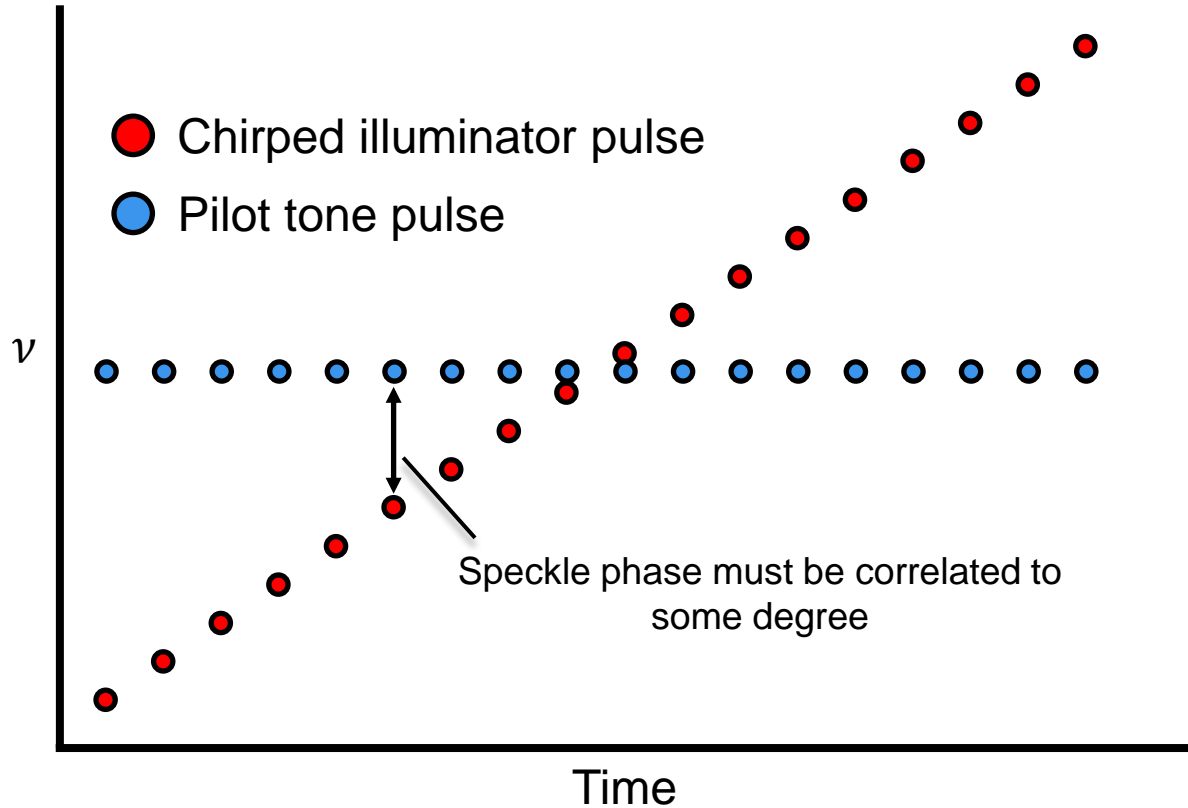
- Flood illuminate distant object with coherent light from **two illuminators**
- Interfere images of object with off-axis reference beams resulting in a **multiplexed hologram**
- Repeat for many frequencies in a narrow bandwidth
- Perform Fourier transform over optical frequency to generate 3D image

## Multiplexed Holograms



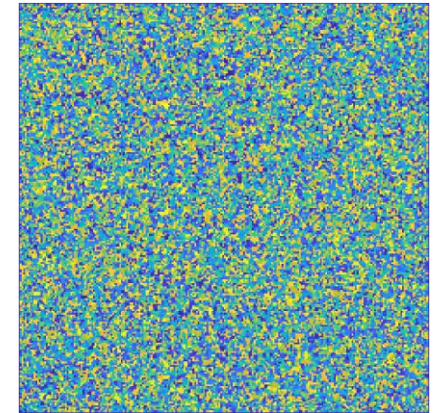
Krause, B. (2017). U.S. Patent No. 9,581,967. Washington, DC: U.S. Patent and Trademark Office.  
 Krause, B. W., Tiemann, B. G., & Gatt, P. (2012). Motion compensated frequency modulated continuous wave 3D coherent imaging lidar with scannerless architecture. *Applied optics*, 51(36), 8745-8761.

# Addition of Brian Krause's pilot tone enables motion compensation

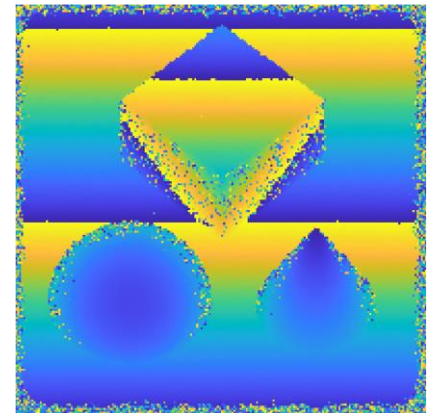


Independent speckle phase pulse-to-pulse  
Pilot tone OFF

Range images



Independent speckle phase pulse-to-pulse  
Pilot tone ON

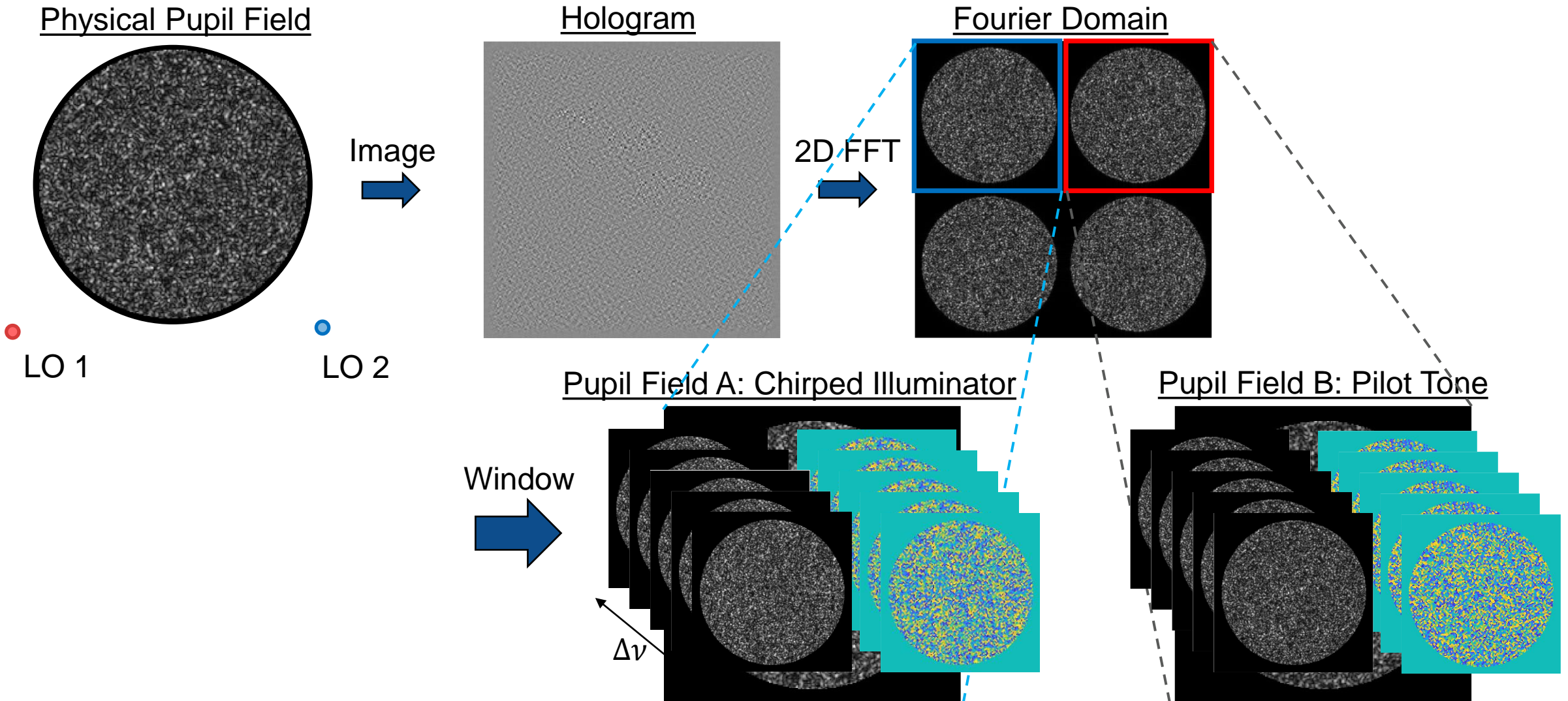


Robust to object motion/vibration

Krause, B. (2017). U.S. Patent No. 9,581,967. Washington, DC: U.S. Patent and Trademark Office.  
 Krause, B. W., Tiemann, B. G., & Gatt, P. (2012). Motion compensated frequency modulated continuous wave 3D coherent imaging ladar with scannerless architecture. *Applied optics*, 51(36), 8745-8761.



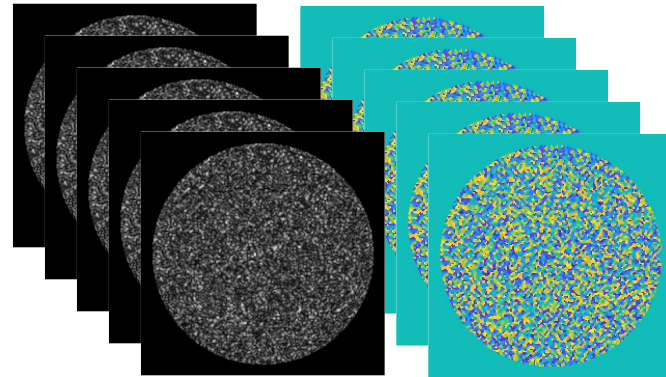
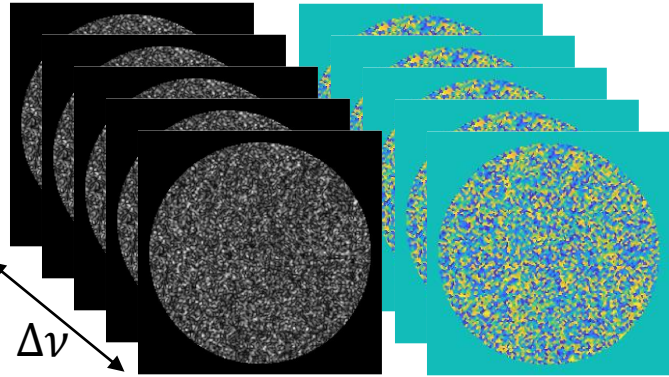
# Processing for multiplexed holograms



# Conjugate product images

Pupil Fields A

Pupil Fields B



2D FFT

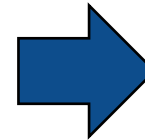
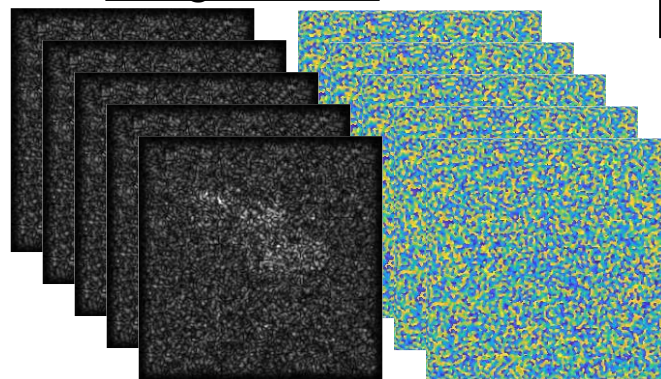
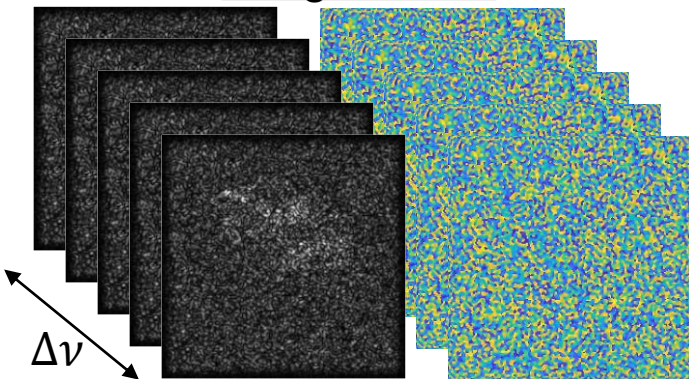


2D FFT

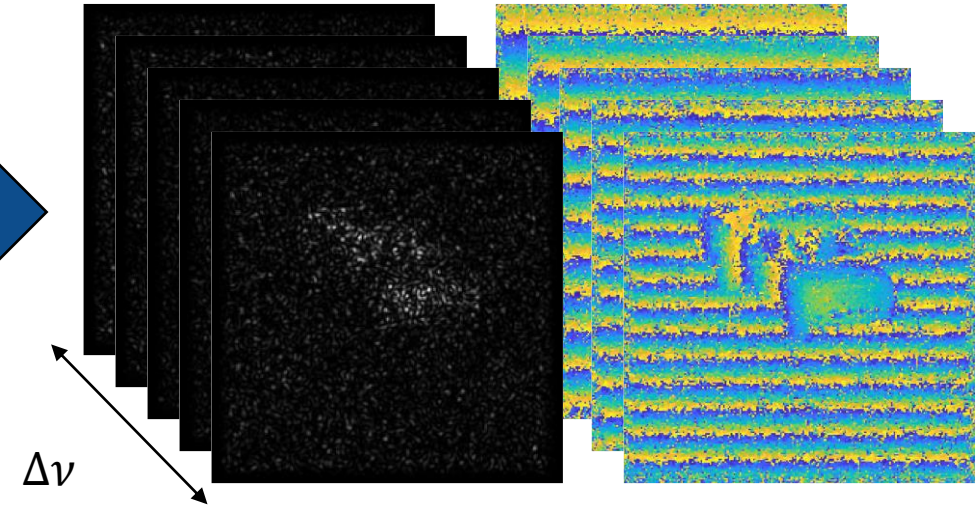


Image Fields A

Image Fields B



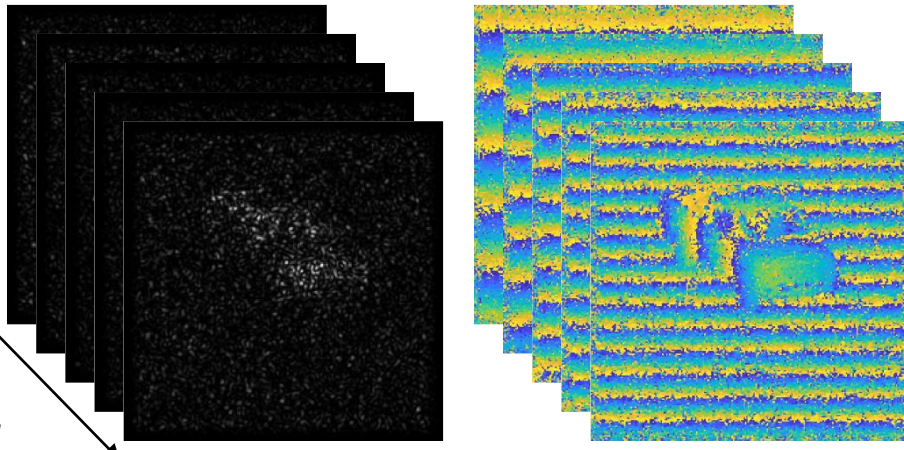
Conjugate Product  
 $AB^*$





# 3D image formation with a pilot tone

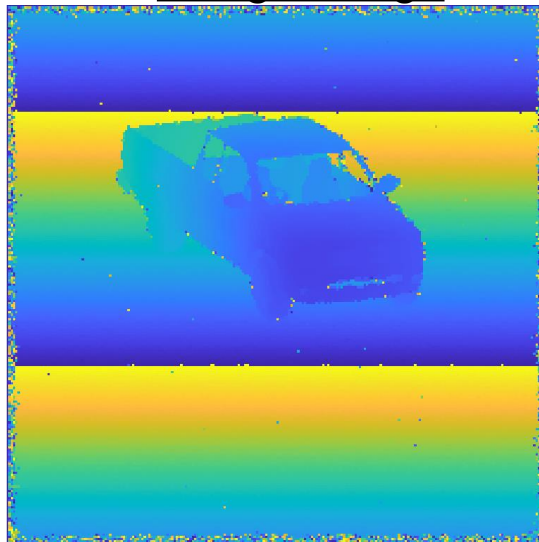
Conjugate Product  $AB^*$



2D Frequency-Averaged Image

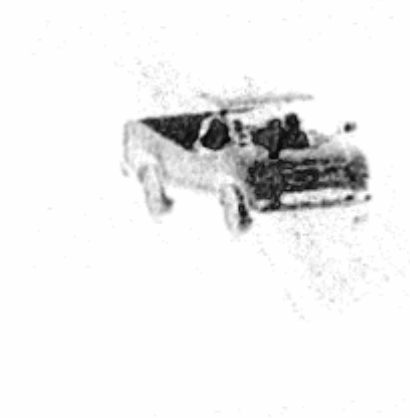


Range Image



3D Irradiance Cloud

1D FFT  
➔



- Range image found by location of max irradiance at each  $x, y$
- Speckle averaging can occur

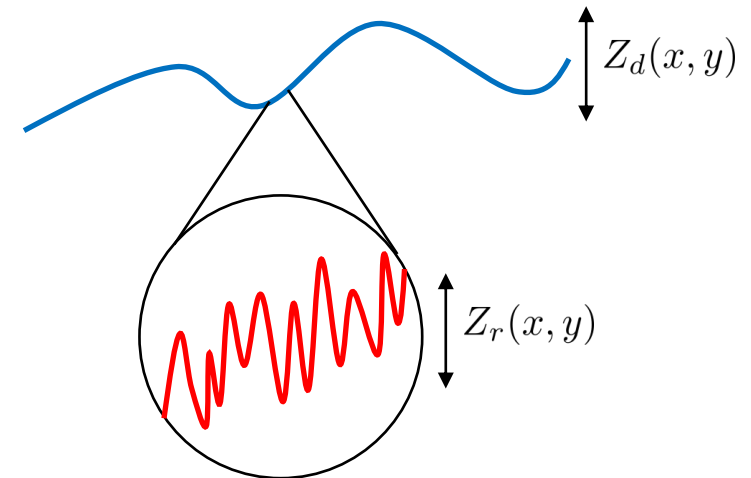
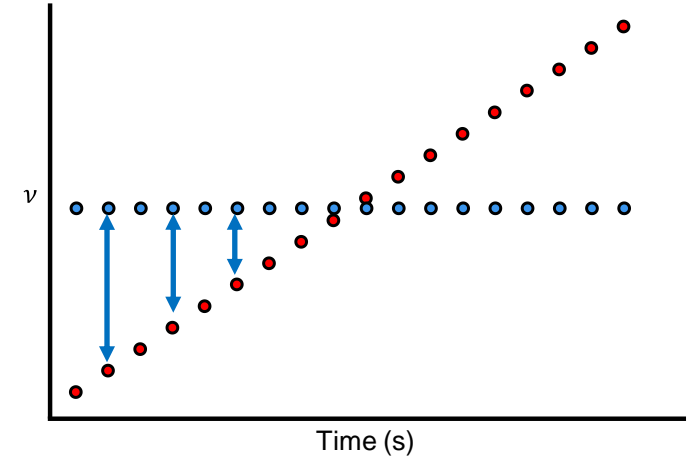
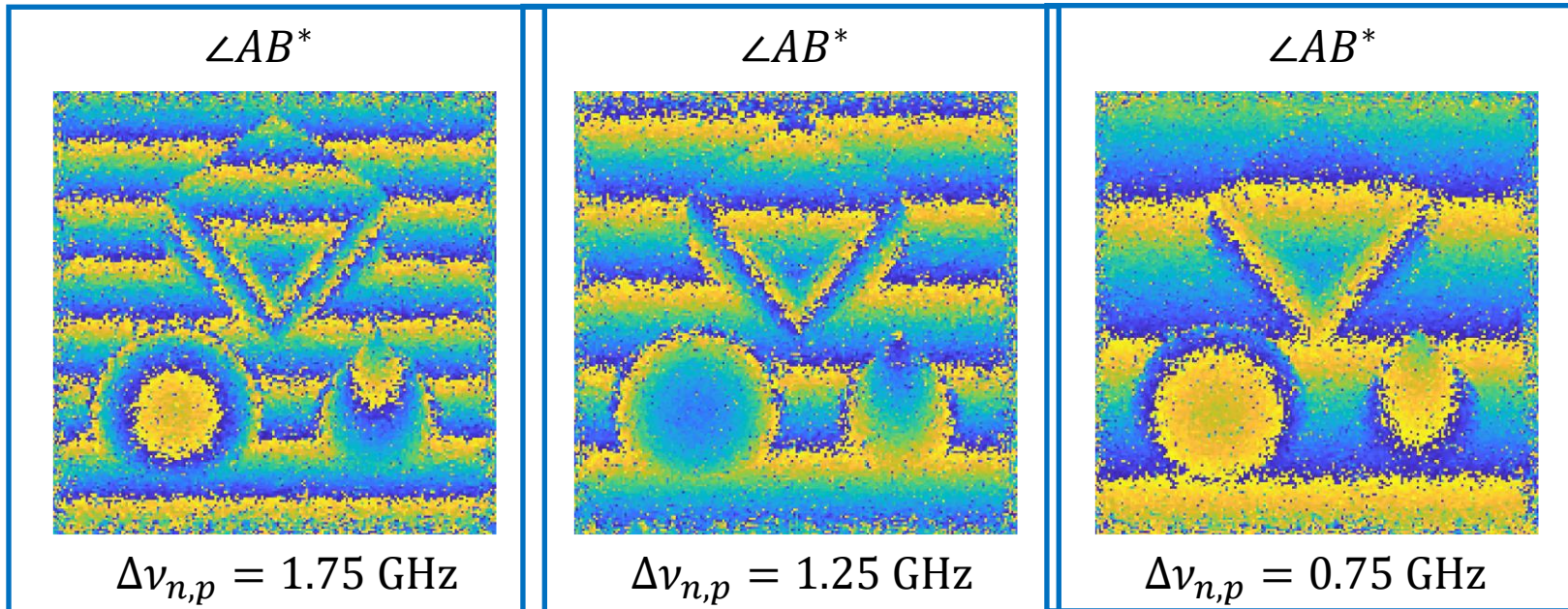
**Speckle averaging occurs when speckle phase is uncorrelated pulse-pair to pulse-pair**



# How does one form a 3D image via conjugate product images?

- Take **conjugate product** of images with in a pulse pair
- Remaining phase shows optical path difference between the chirped illuminator and pilot tone

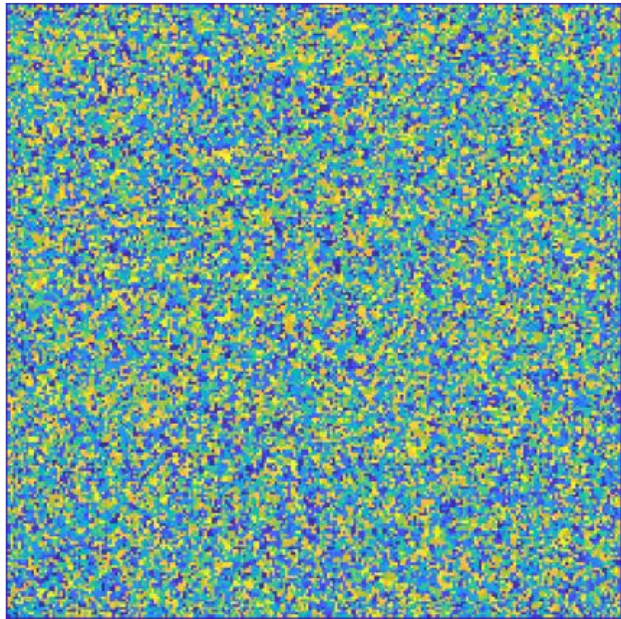
$$E_n(u, v; \nu_n - \nu_p) = U_n(u, v; \nu_n)U_{n,pilot}^*(u, v; \nu_p)$$



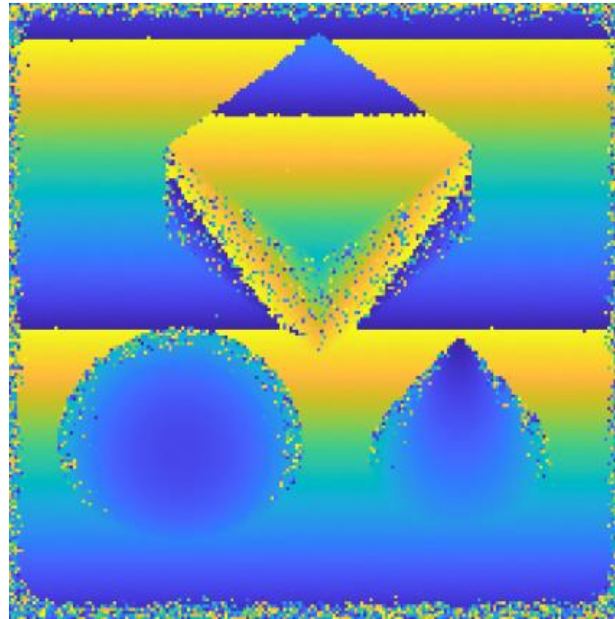


# With pilot-tone 3D imaging, range chatter can appear for sloped object facets

Range image formed w/o pilot tone



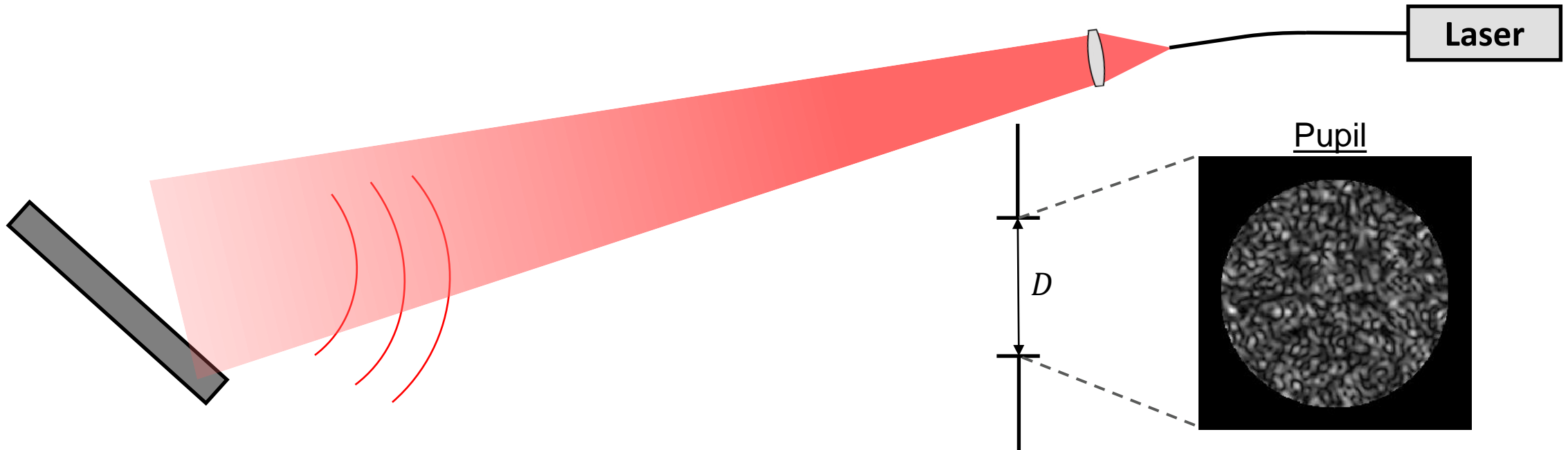
Range image formed w/ pilot tone



Spoiler confirmed:  
Range chatter is due to speckle phase changing with frequency due purely to *diffraction*

**Range chatter can appear over sloped object facets for even in the case of infinite SNR!**

# Speckle shifting for sloped objects: Changing tilt

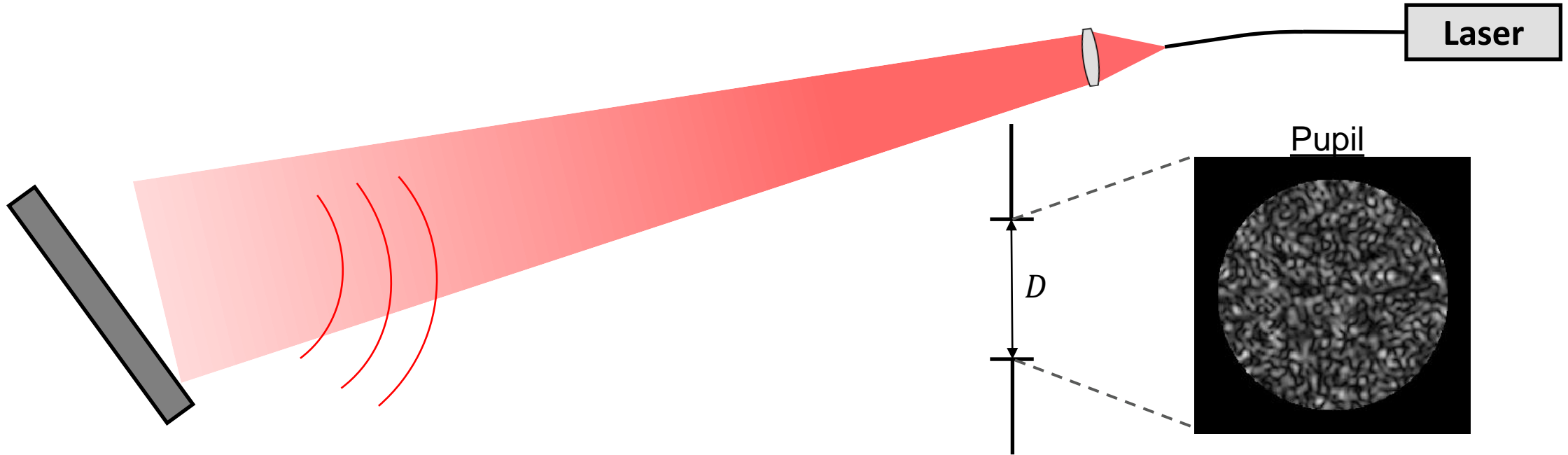


**Speckle pattern in pupil shifts with object tilt**





# Speckle shifting for sloped objects: Changing frequency causes speckle decorrelation



**Speckle pattern in pupil  
shifts with changing frequency**

# Defining the object phase difference for two illumination frequencies

- Define a frequency difference within a pair of frequencies  $\nu_1$  and  $\nu_2$ ,  $|\nu_1 - \nu_2| = \Delta\nu_{1,2}$

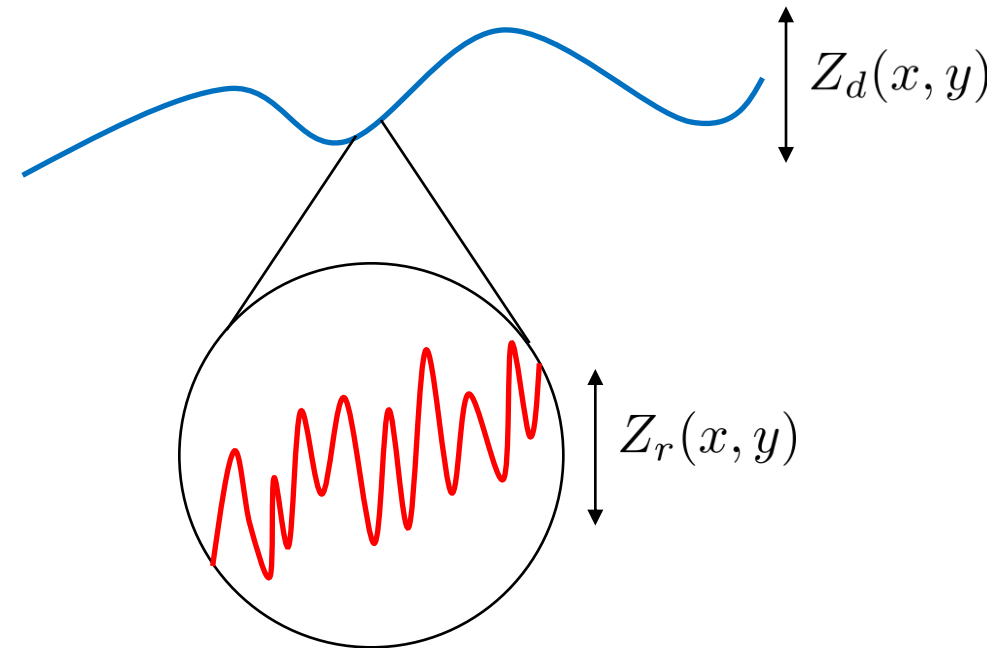
$$A(\xi, \eta) \exp[i\phi(\xi, \eta)]$$

$$\phi(\xi, \eta) = \frac{4\pi\nu}{c} [z_0 + Z_d(\xi, \eta) + Z_r(\xi, \eta)]$$

- Change in phase,  $\Delta\phi(x, y)$  between two frequencies is

$$\Delta\phi(\xi, \eta) = \frac{4\pi}{c} [\cancel{\Delta\nu_{1,2}z_0} + \Delta\nu_{1,2}Z_d(\xi, \eta) + \cancel{\Delta\nu_{1,2}Z_r(\xi, \eta)}]$$

$$\Delta\phi(\xi, \eta) = \frac{4\pi}{c} \Delta\nu_{1,2}Z_d(\xi, \eta)$$





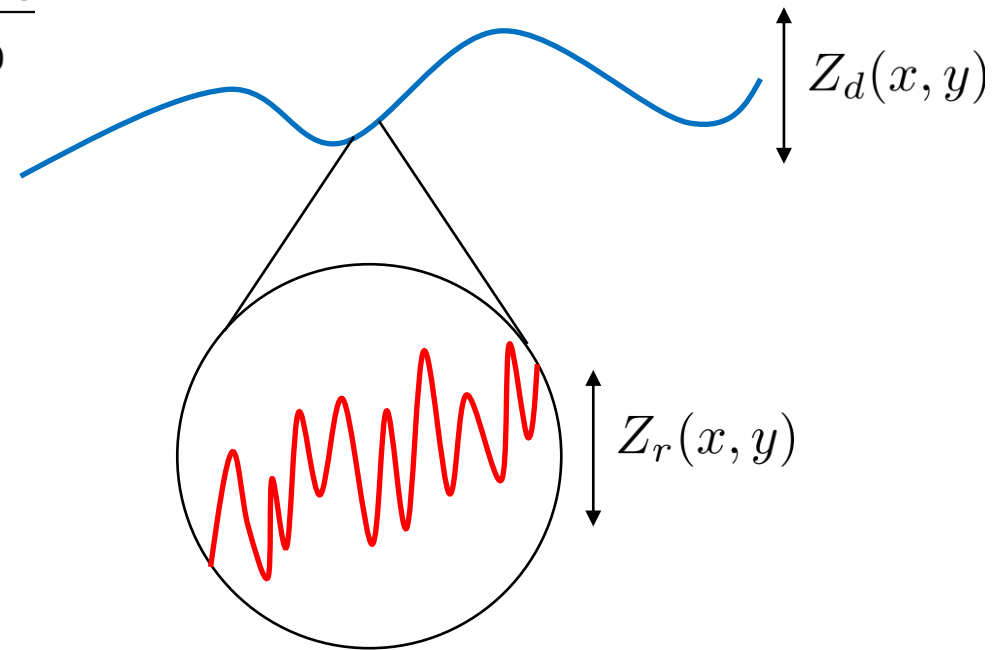
# Speckle decorrelation in terms of the slope bandwidth product (SBP)

- Assume  $Z_d(x, y) = \alpha x$ , a linearly sloped object. Then the  $\Delta\phi(x, y)$  yields speckle shift of  $\Delta x$  via **Fourier shift theorem**

$$\frac{4\pi}{c} \Delta\nu_{1,2} Z_d(\xi, \eta) = \frac{4\pi}{c} \Delta\nu_{1,2} \alpha \xi = 2\pi \Delta x f_\xi \Big|_{f_\xi = \xi / (\lambda_0 z_0)} = \frac{2\pi \Delta x \xi}{\lambda_0 z_0}$$

- Taking  $\lambda_0 \approx c/\nu_0$

$$\text{SBP} = \boxed{\alpha \frac{\Delta\nu_{1,2}}{\nu_0} = \frac{\Delta x}{2z_0}}$$

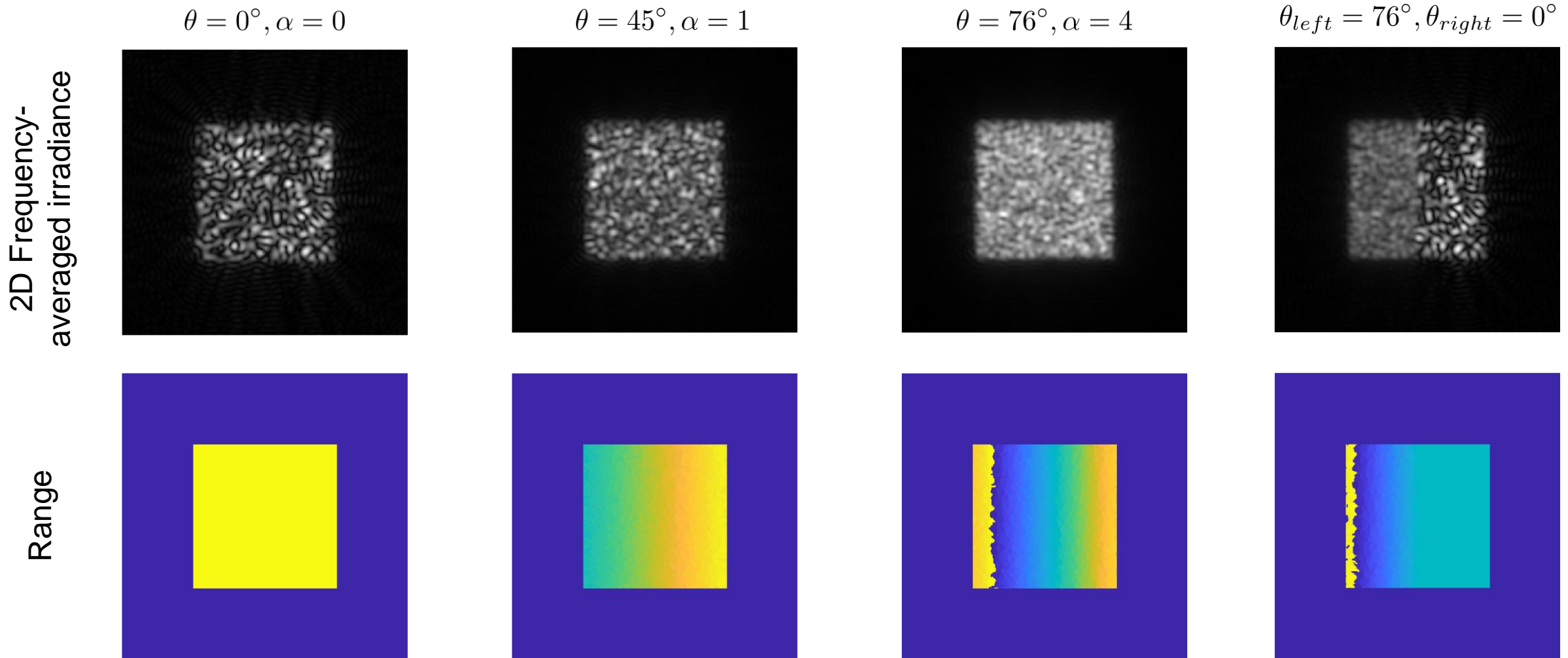


Banet, M. T., & Fienup, J. R. (2023). Speckle decorrelation effects on motion-compensated, multi-wavelength 3D digital holography: theory and simulations. *Optical Engineering*, 62(7), 073103-073103.



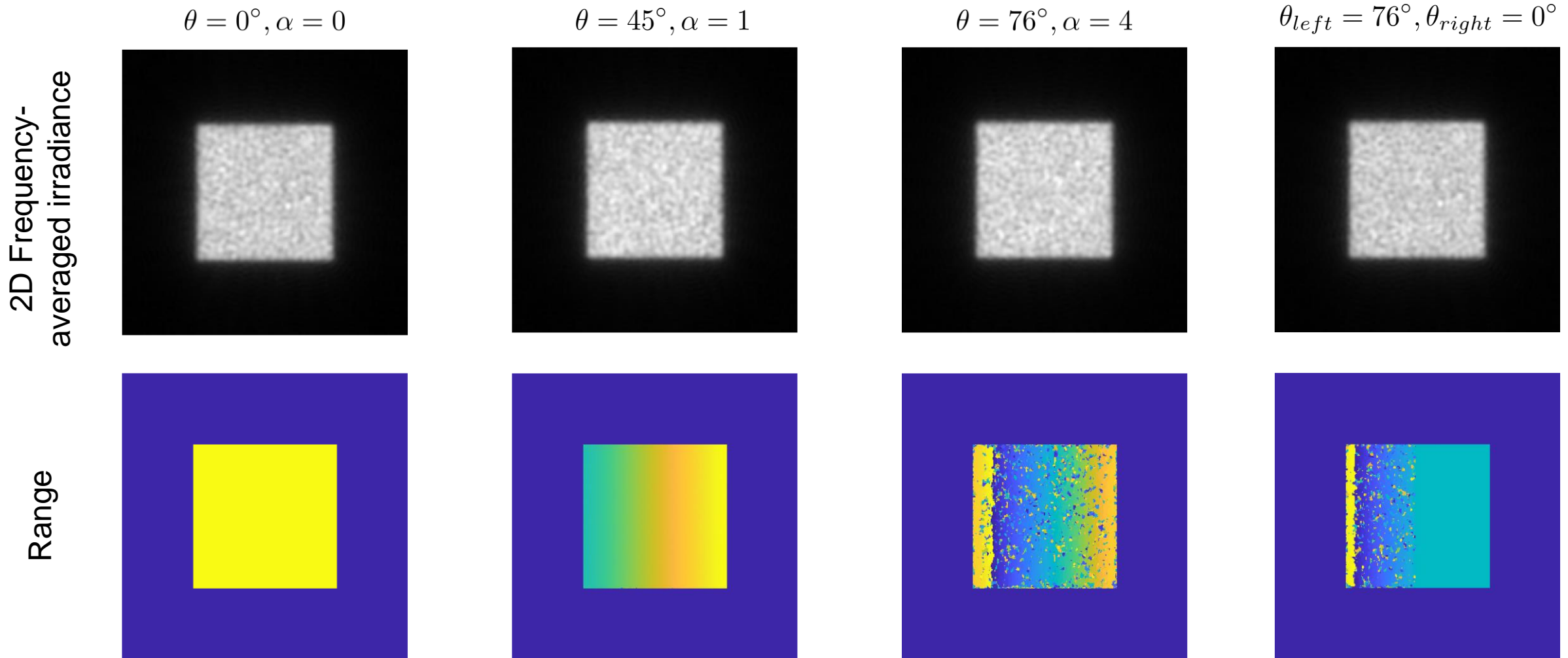


# Independent speckle phase pulse-pair to pulse-pair: Conventional 3D imaging



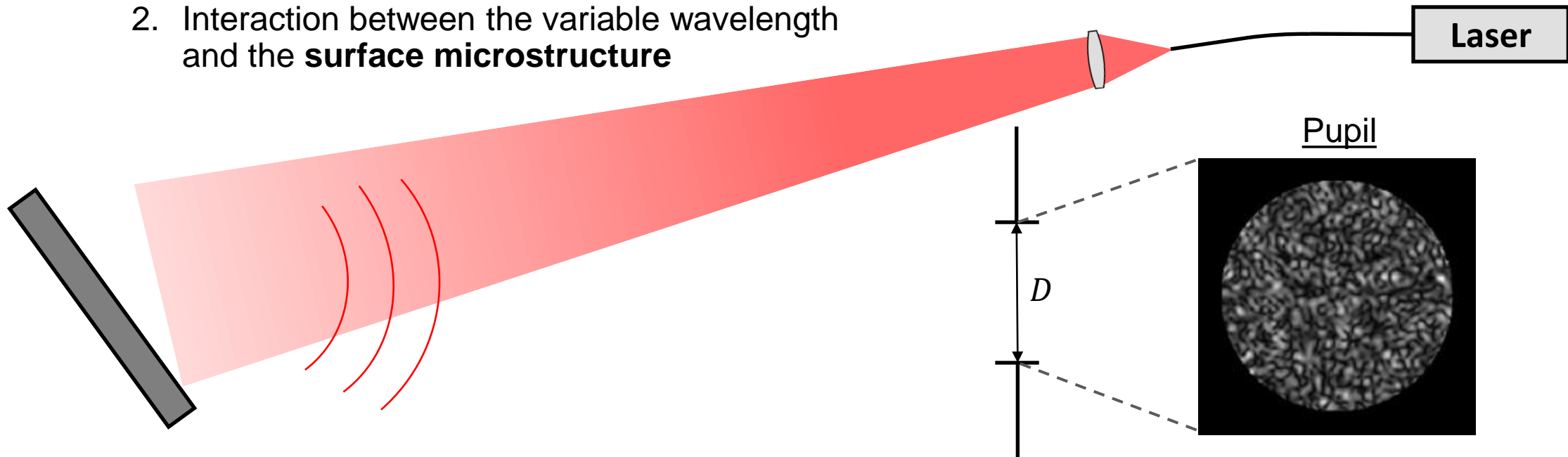


# Common or correlated speckle phase pulse-to-pulse: Pilot-tone 3D imaging



# How does changing wavelength change speckle?

- Speckle evolves with changes in wavelength via two mechanisms:<sup>†</sup>
  1. Changes due to the Fresnel **diffraction** integral as a function of wavelength
  2. Interaction between the variable wavelength and the **surface microstructure**

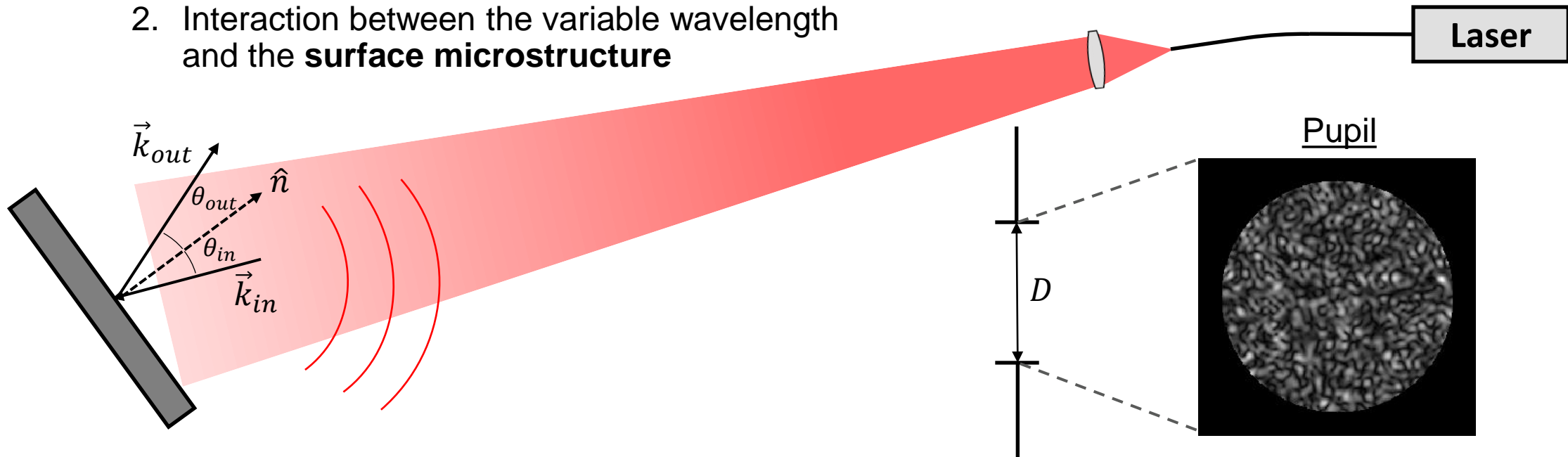


<sup>†</sup> Goodman, Joseph W., Speckle Phenomena in Optics: Theory and Applications, 2nd ed., SPIE Press, Bellingham, Washington, United States (2020).



# What about changes in wavelength?

- Speckle evolves with changes in wavelength via two mechanisms:<sup>†</sup>
  1. Changes due to the Fresnel **diffraction** integral as a function of wavelength
  2. Interaction between the variable wavelength and the **surface microstructure**

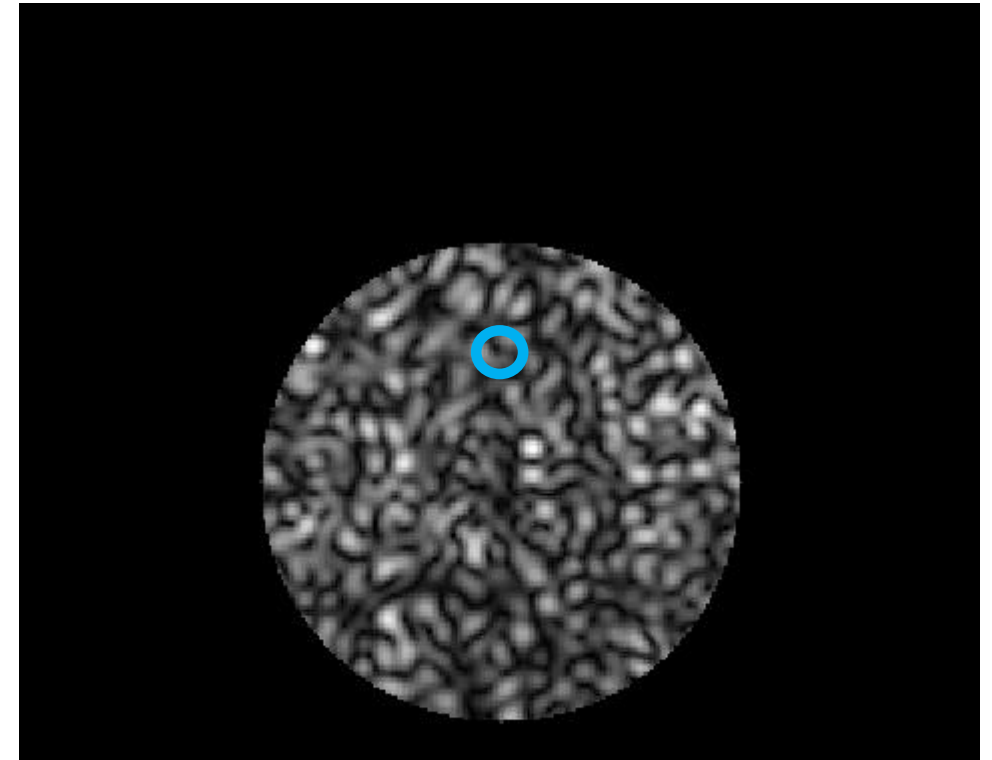
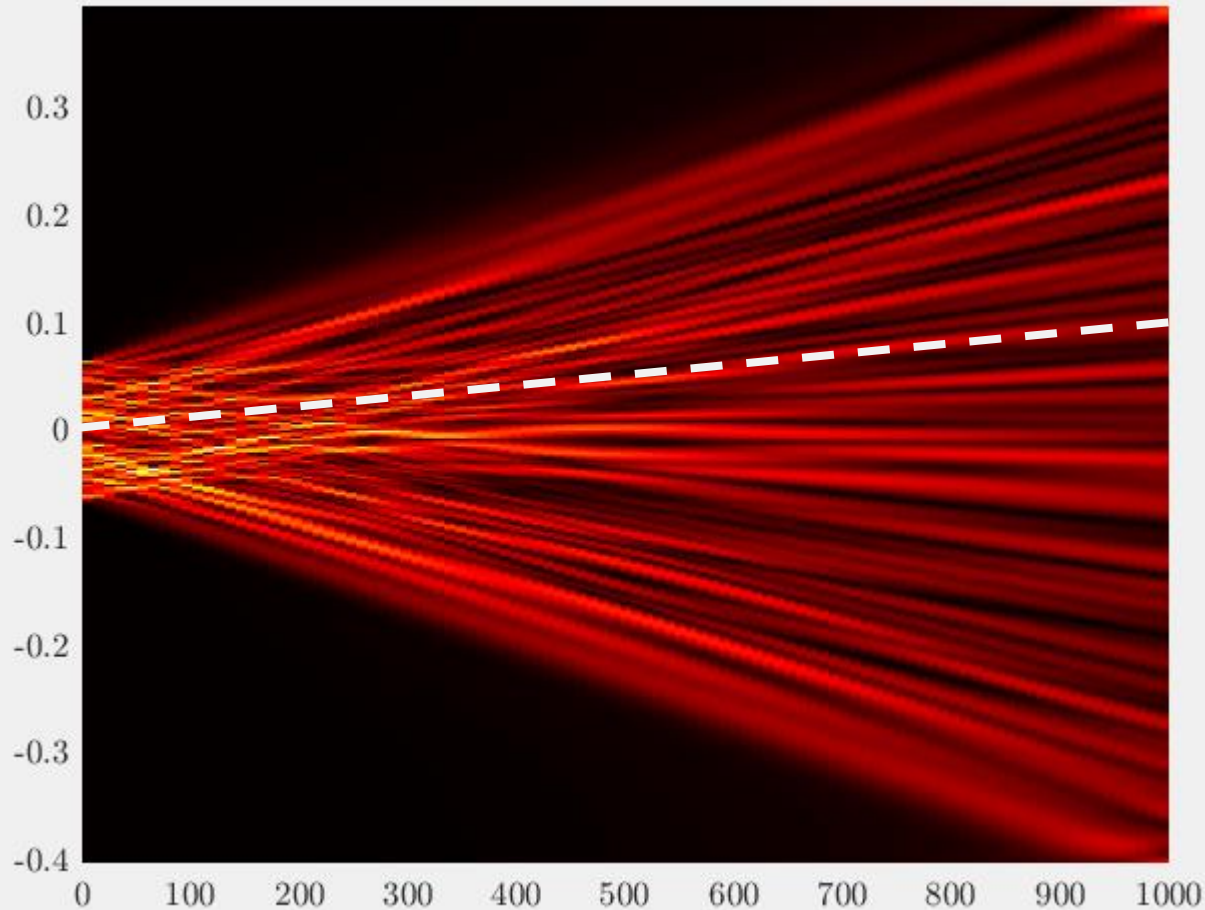


<sup>†</sup> Goodman, Joseph W., Speckle Phenomena in Optics: Theory and Applications, 2nd ed., SPIE Press, Bellingham, Washington, United States (2020).



# Speckles contracting/expanding for a sloped object (small slope, large bandwidth)

Irradiance profile view

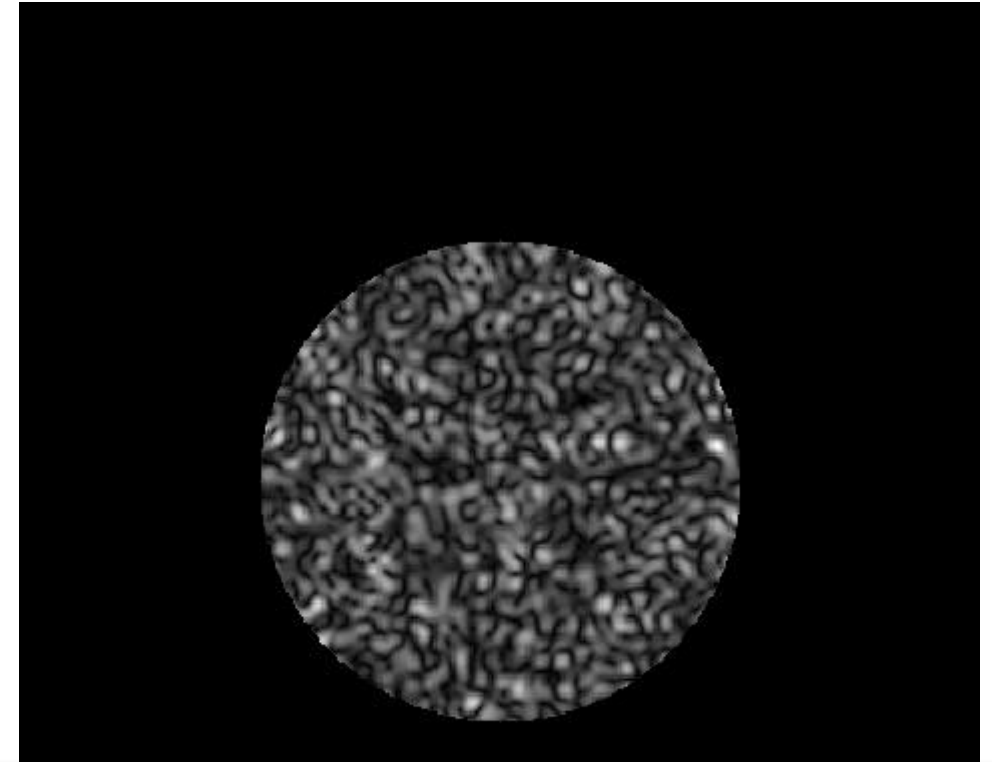
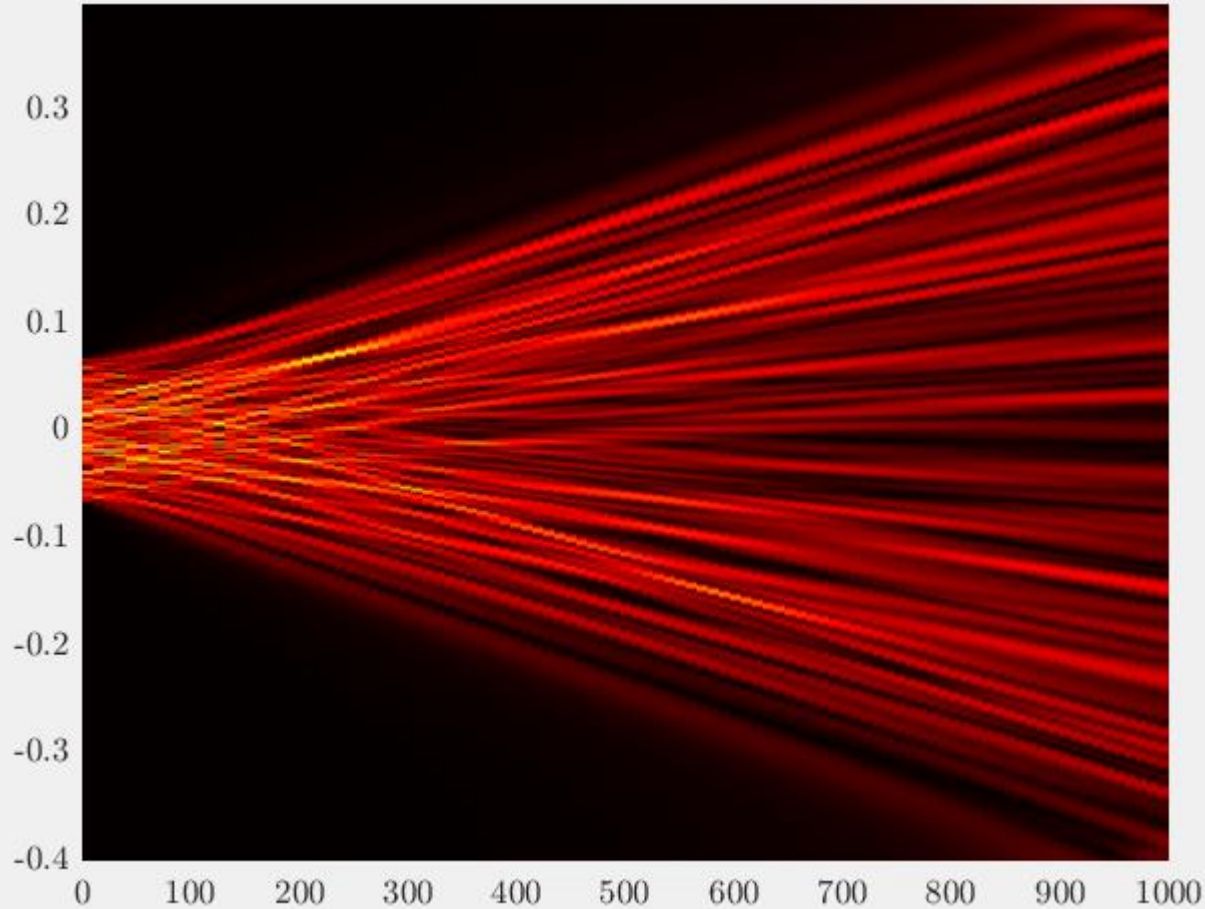


**Speckle pattern in pupil contracts/expands with changing wavelength**



# Speckles translating for a sloped object (large slope, small bandwidth)

Irradiance profile view

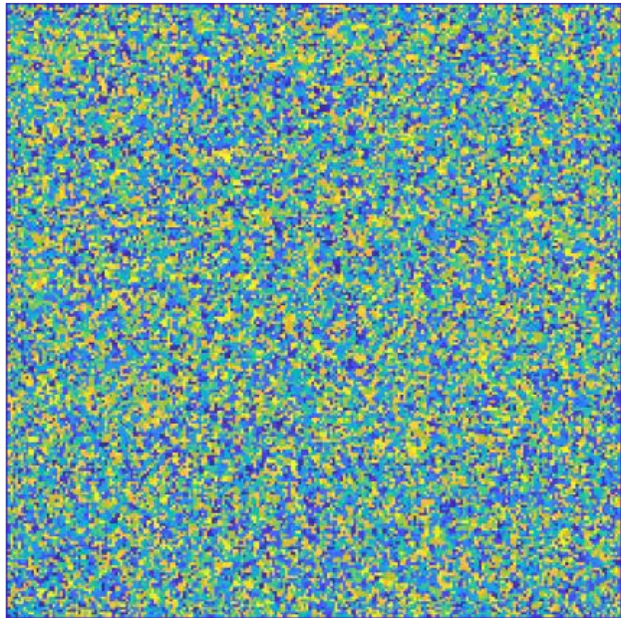


**Speckle pattern in pupil translates with  
changing wavelength**

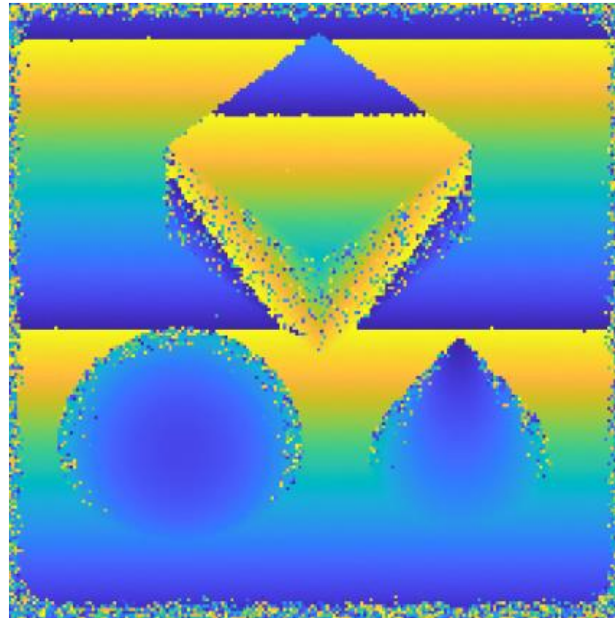


# How can we alleviate range chatter?

Range image formed w/o pilot tone



Range image formed w/ pilot tone



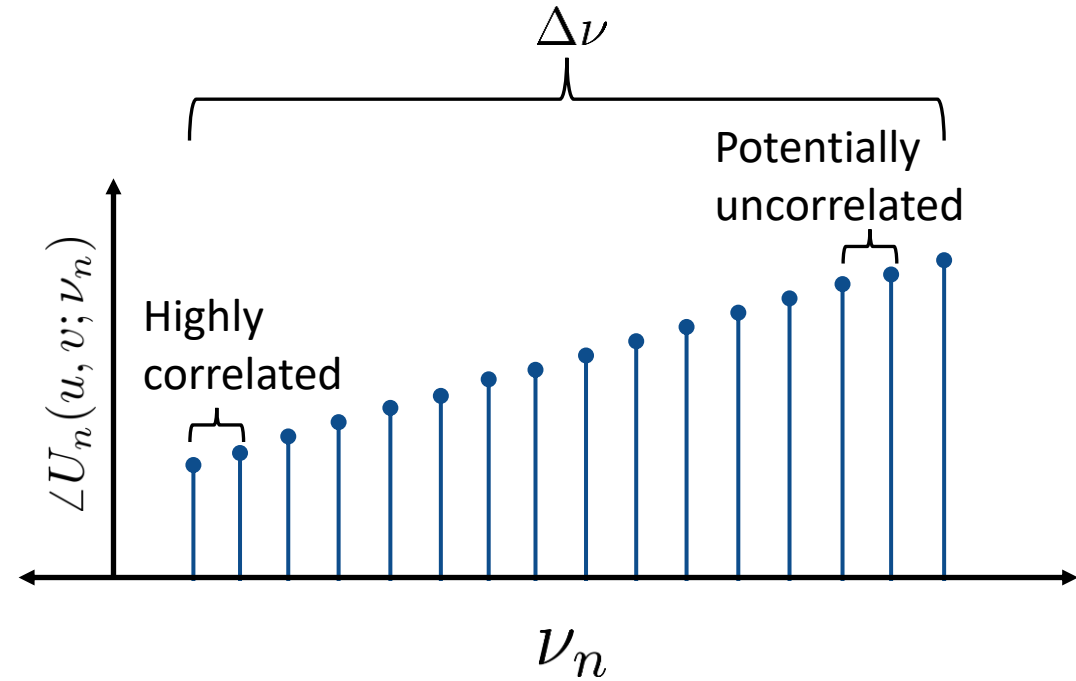
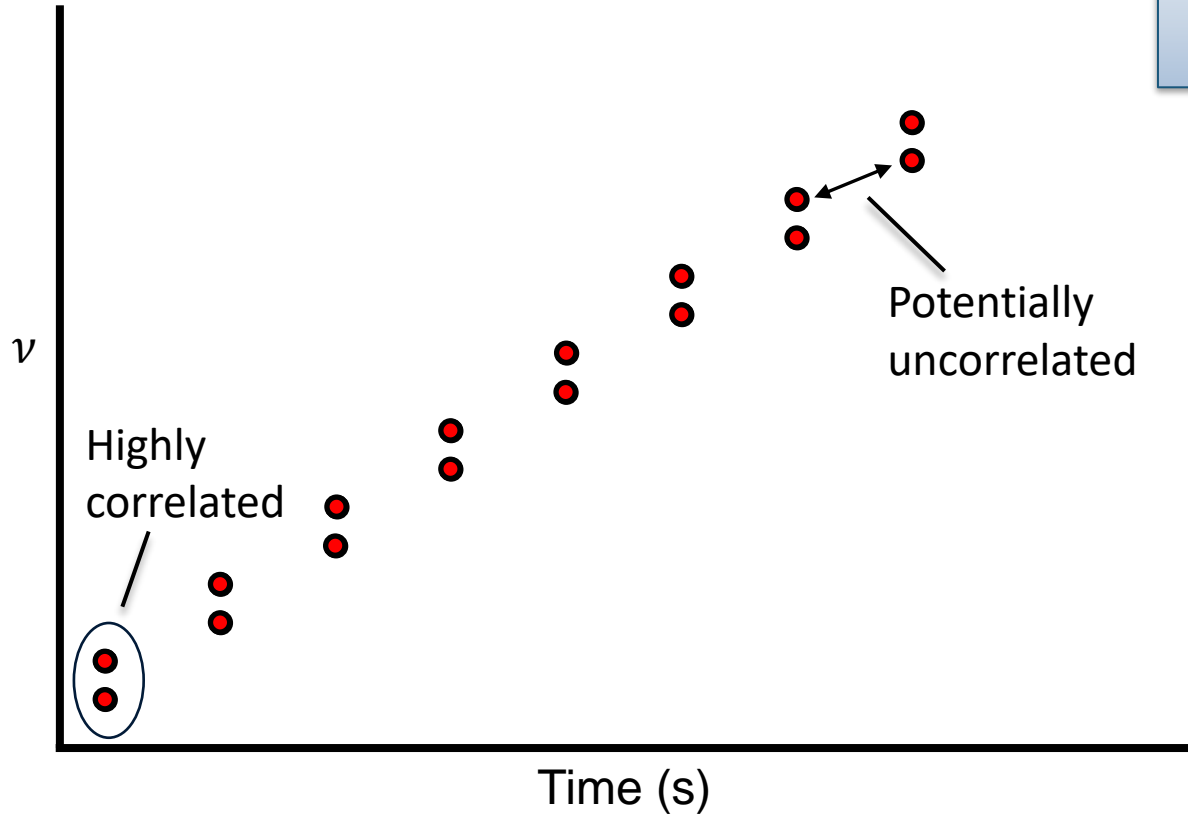
Spoiler confirmed:  
Range chatter is due to speckle phase changing with frequency due purely to *diffraction*

**Range chatter can appear over sloped object facets even in the case of infinite SNR!**



# Dual tone 3D imaging

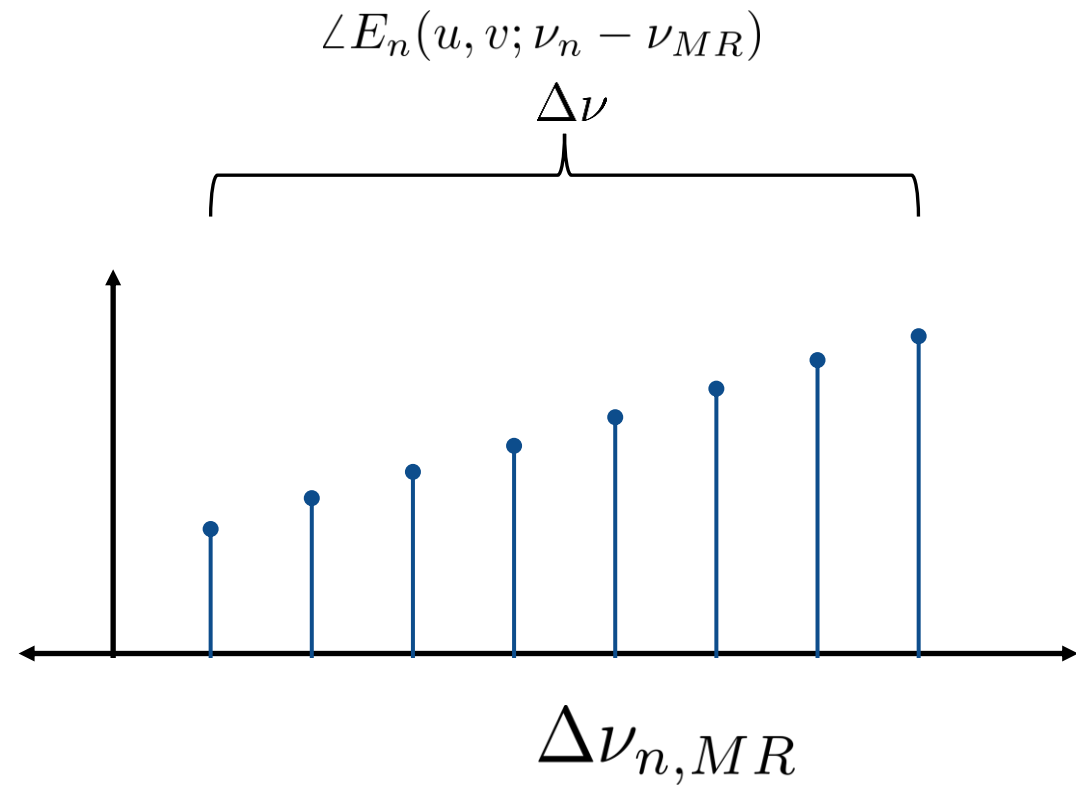
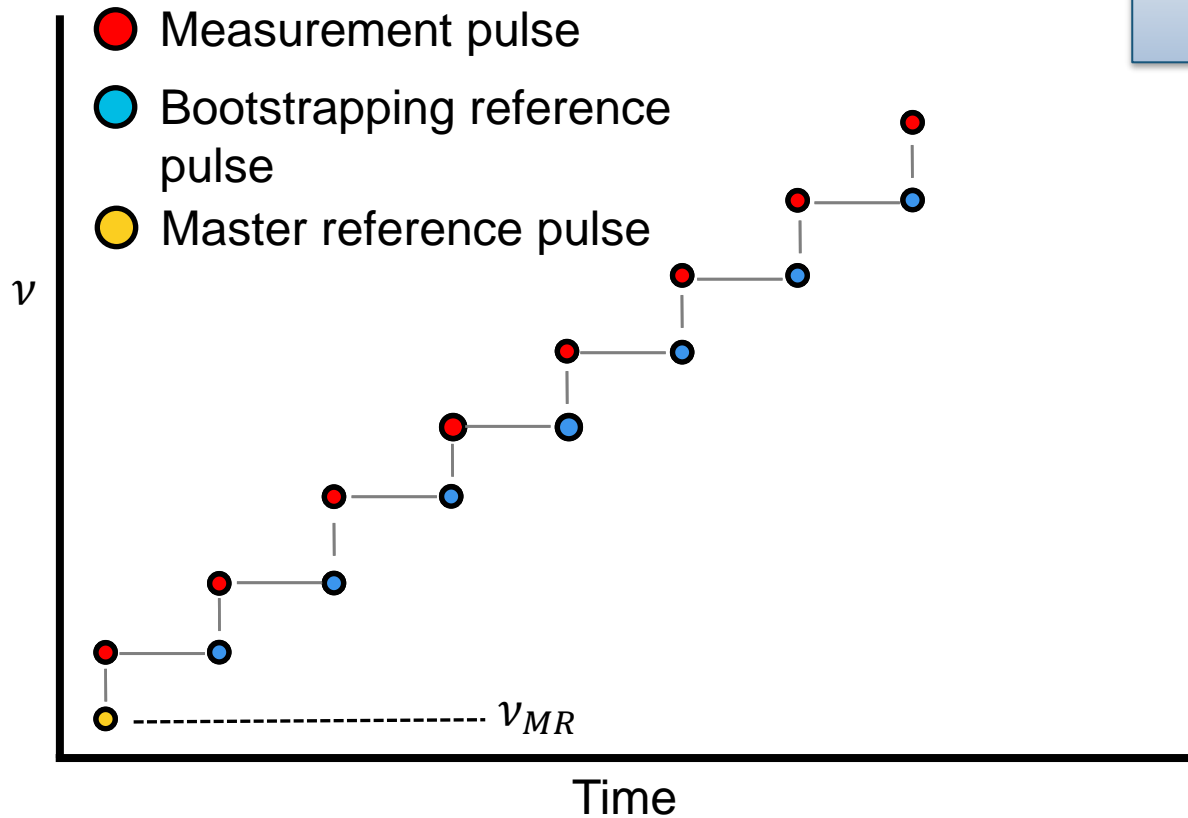
**Speckle phase is highly correlated within pulse pairs**



**Total number of samples in optical frequency domain,  $S = 16$**

# Stairstep 3D imaging: pulse configuration

**Redundant frequency measurements  
sample frequency-difference space**





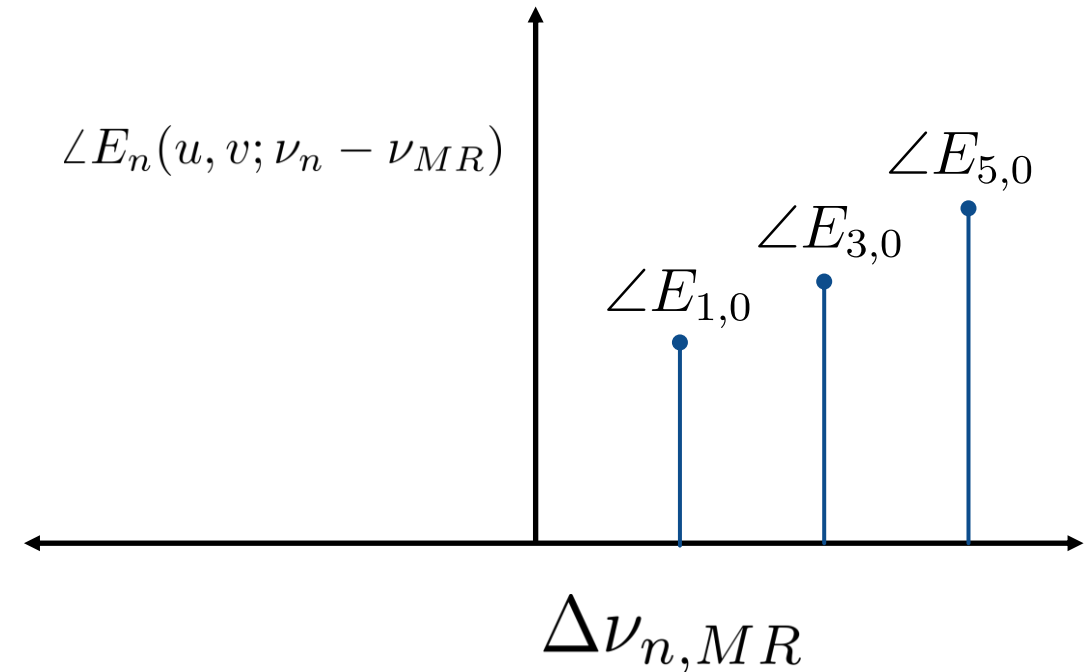
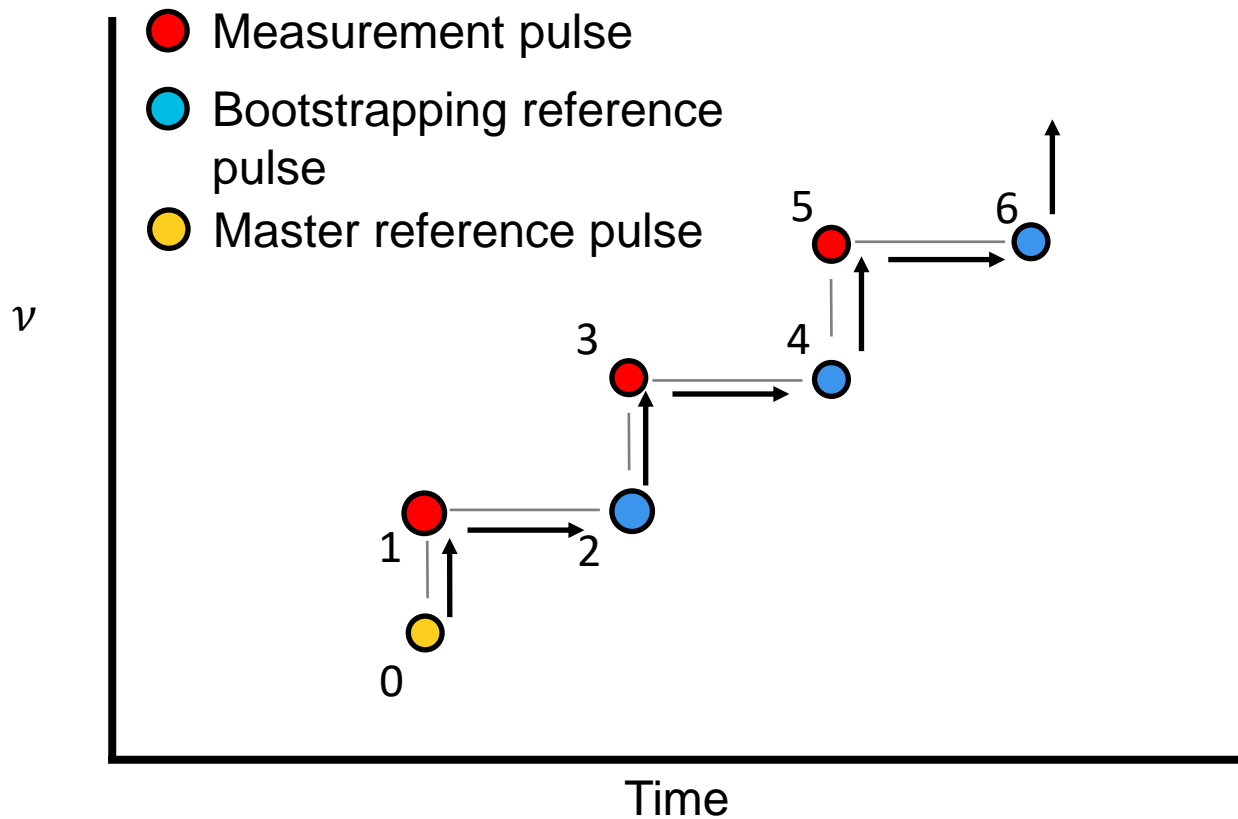


# Stairstep 3D imaging: frequency difference images

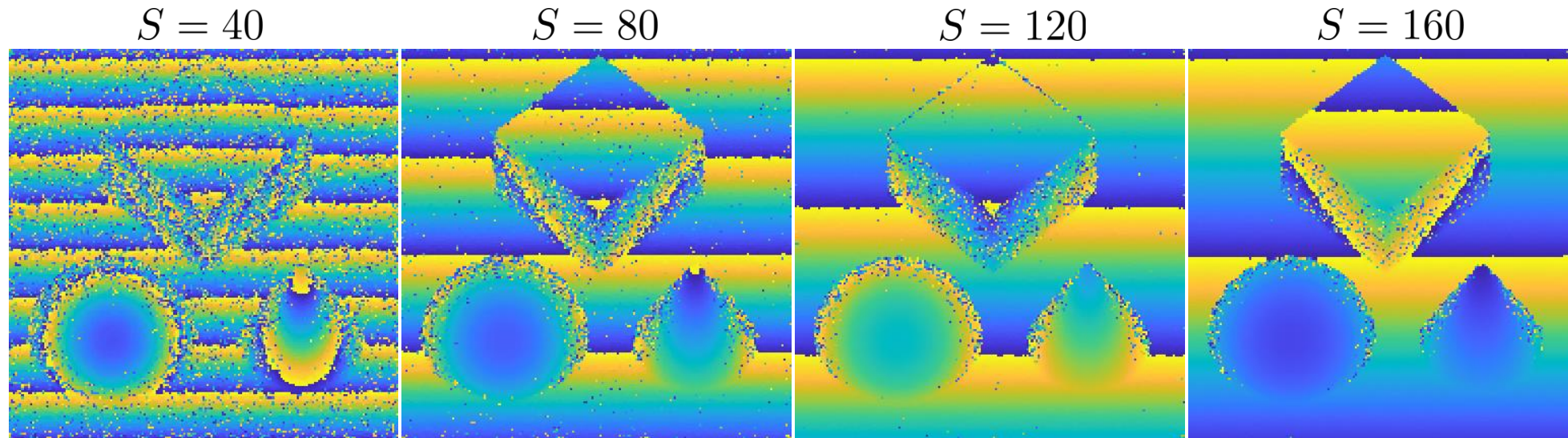
$$U(u, v; \nu) \approx A(u, v) \exp(i4\pi\nu z_0/c) \exp[i4\pi\nu Z_d(u, v)/c] \exp[i\phi_r(u, v)]$$

$$\angle E_{1,0} = \angle U_1 U_0^*$$

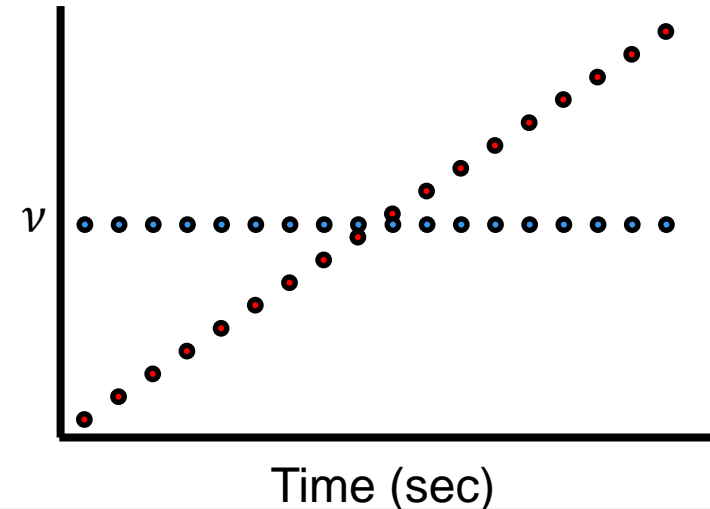
$$\angle E_{3,0} = \angle U_3 U_2^* U_1 U_0^*$$



# Wrapped range images: pilot-tone 3D imaging

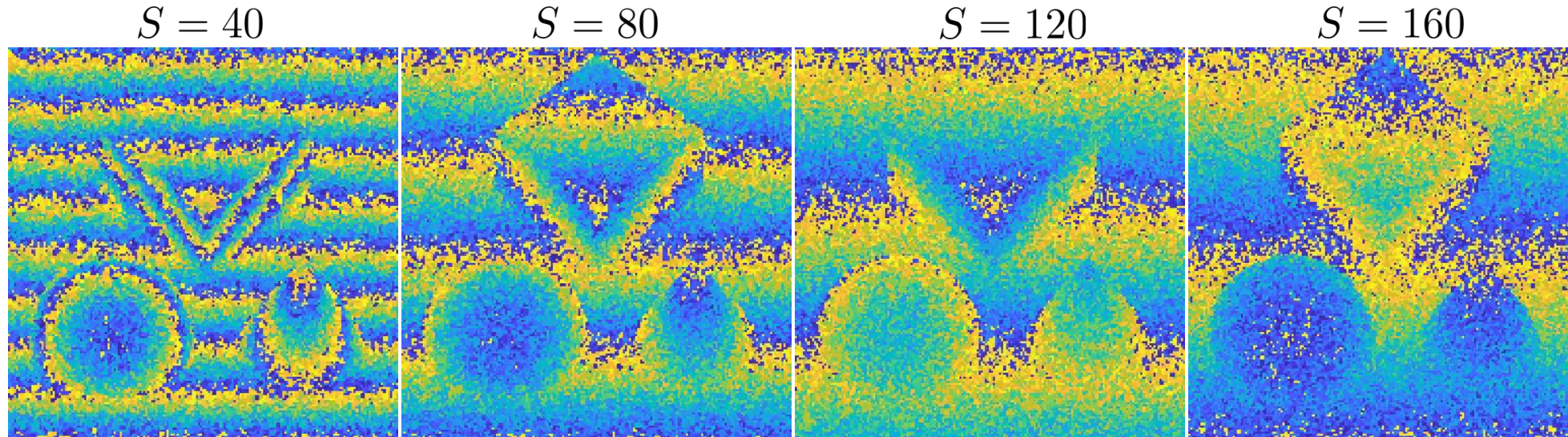


**Pilot-tone images robust to object motion but feature range chatter over highly sloped facets**

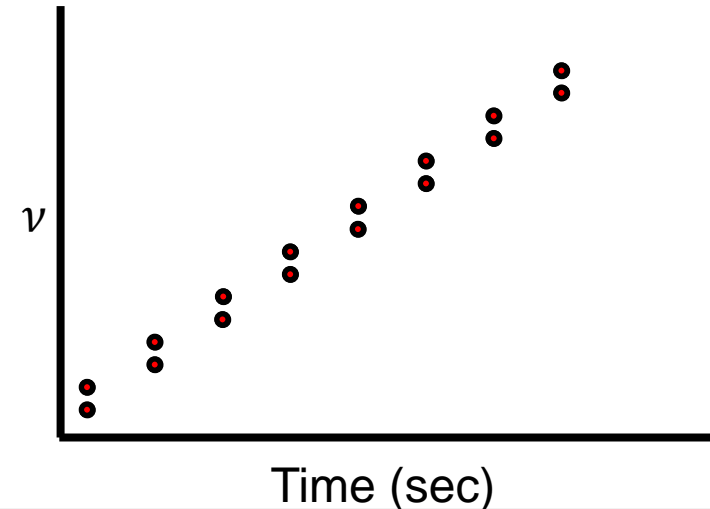




# Wrapped range images: dual-tone 3D imaging

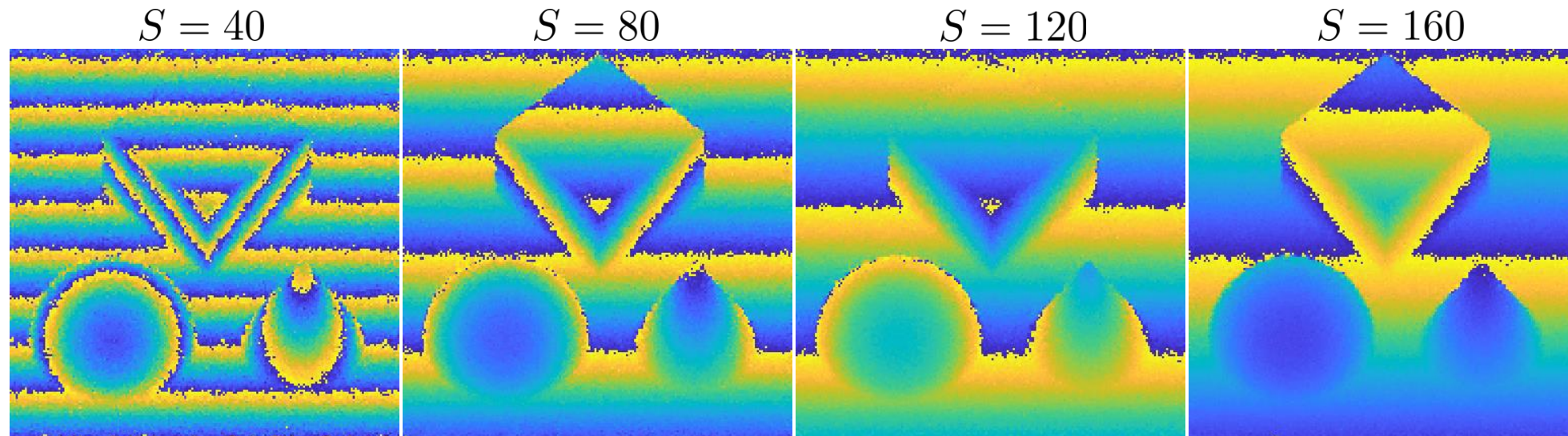


**Dual-tone images feature consistent range errors over the image due to object motion**

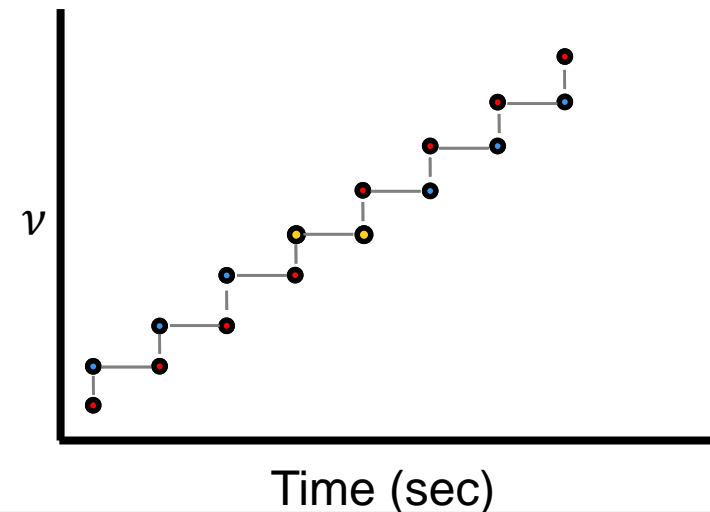




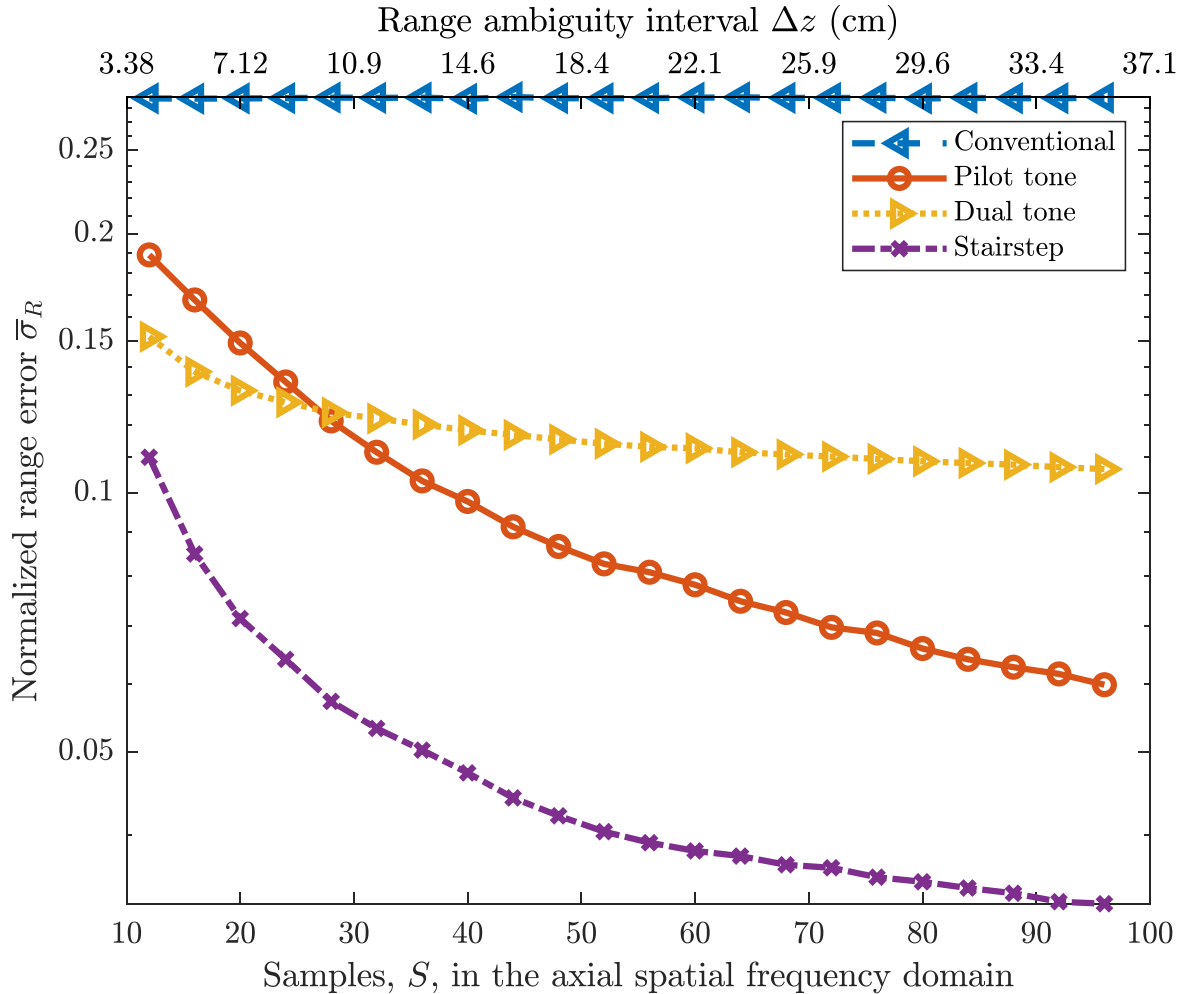
# Wrapped range images: stairstep 3D imaging



**Stairstep images are relatively error free**



# Quantitative results for wrapped range images



## Normalized Wrapped Range Image Error

$$\bar{\sigma}_R = (\text{std}_{u,v \in W(u,v)} \{R_e(u,v)\}) / \Delta z$$

$$R_e(u,v) = \text{mod} \left[ \hat{R}(u,v) - R(u,v) + \Delta z/2, \Delta z \right] - \Delta z/2$$

Range image

Truth range image

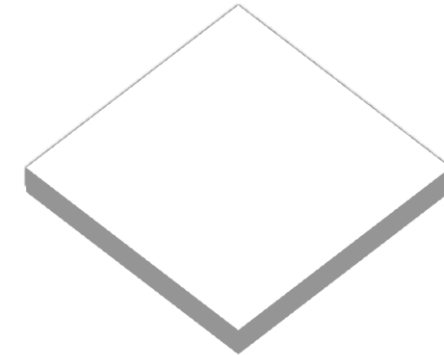
**Stairstep 3D imaging performs the best given infinite SNR**

Banet, M. T., Idris, A., & Fienup, J. R. (2023, October). Multiplexed, multi-wavelength 3D digital holographic imaging methods with range unwrapping. In *Unconventional Imaging, Sensing, and Adaptive Optics 2023* (Vol. 12693, pp. 12-24). SPIE.

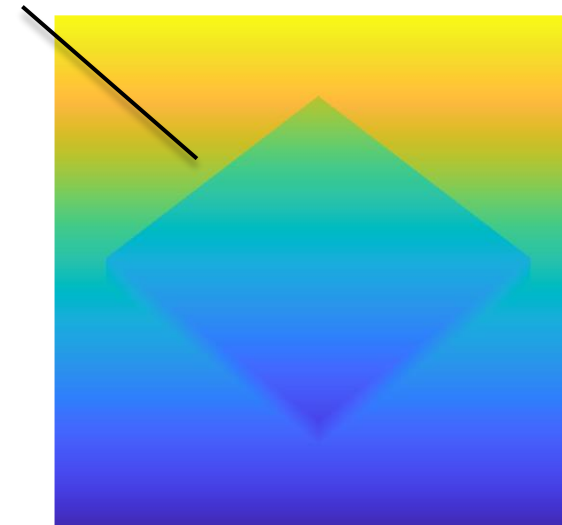
# Simulation trade space for unwrapped range images

- Three 3D imaging modalities
  - Pilot-tone 3D imaging
  - Dual-tone 3D imaging
  - Stairstep 3D imaging
- Keep bandwidth,  $\Delta\nu$ , constant and vary number of samples in optical frequency domain,  $S$
- Enforce independent surface roughness realizations at each timestep

**Maximum range discontinuity  
determines unwrapping performance**

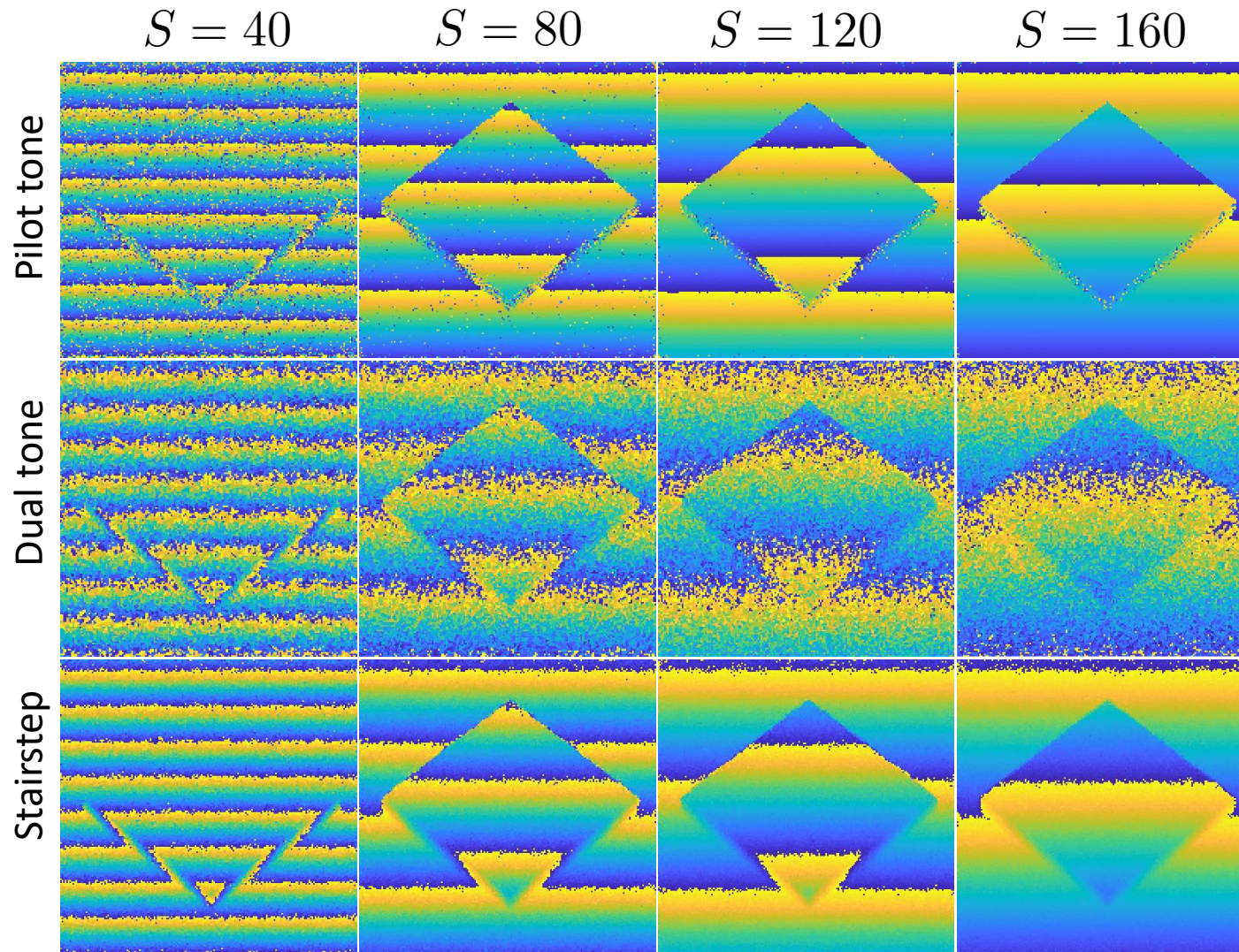


Max discontinuity  
of 8.5 cm



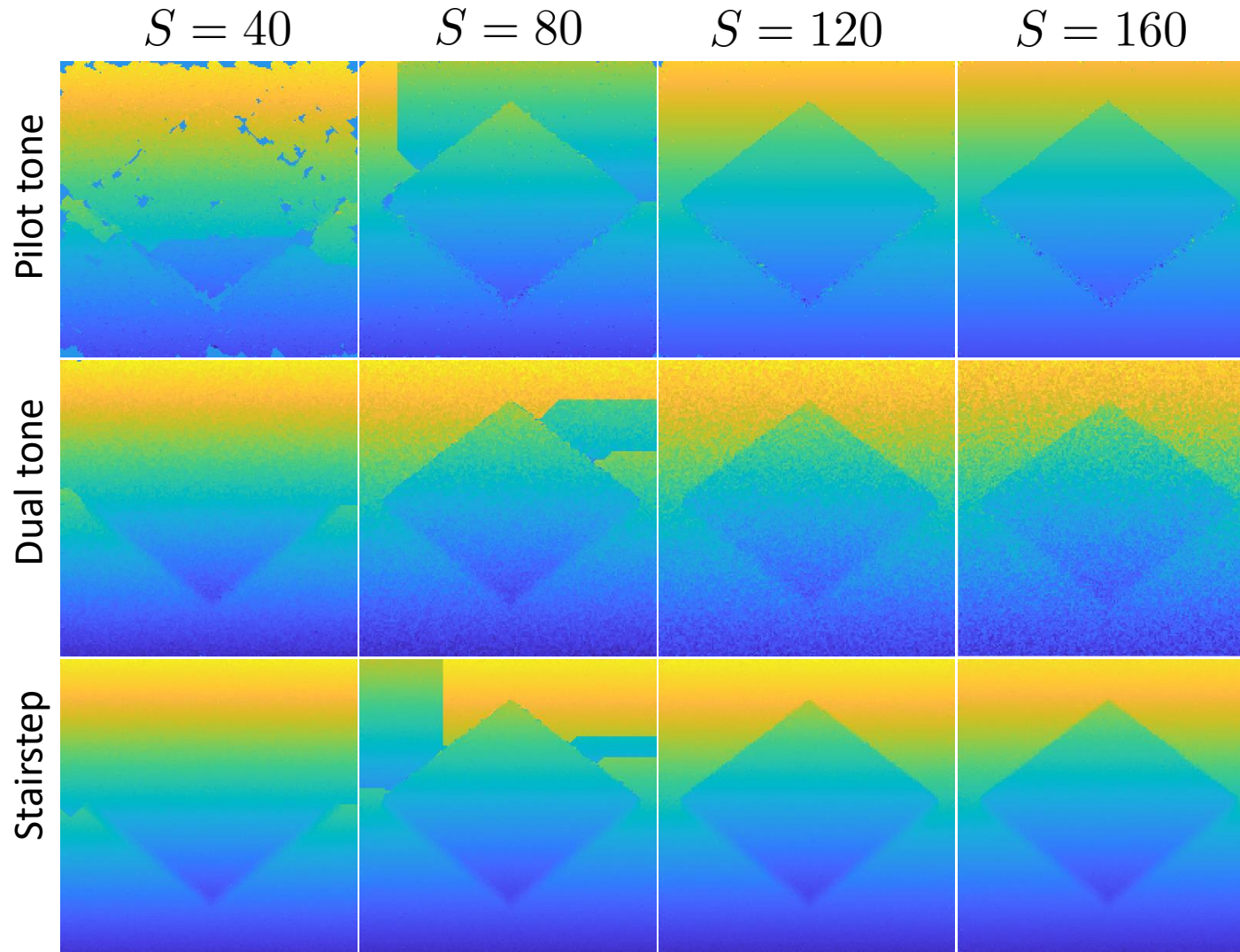


# Wrapped range images: raised square plate

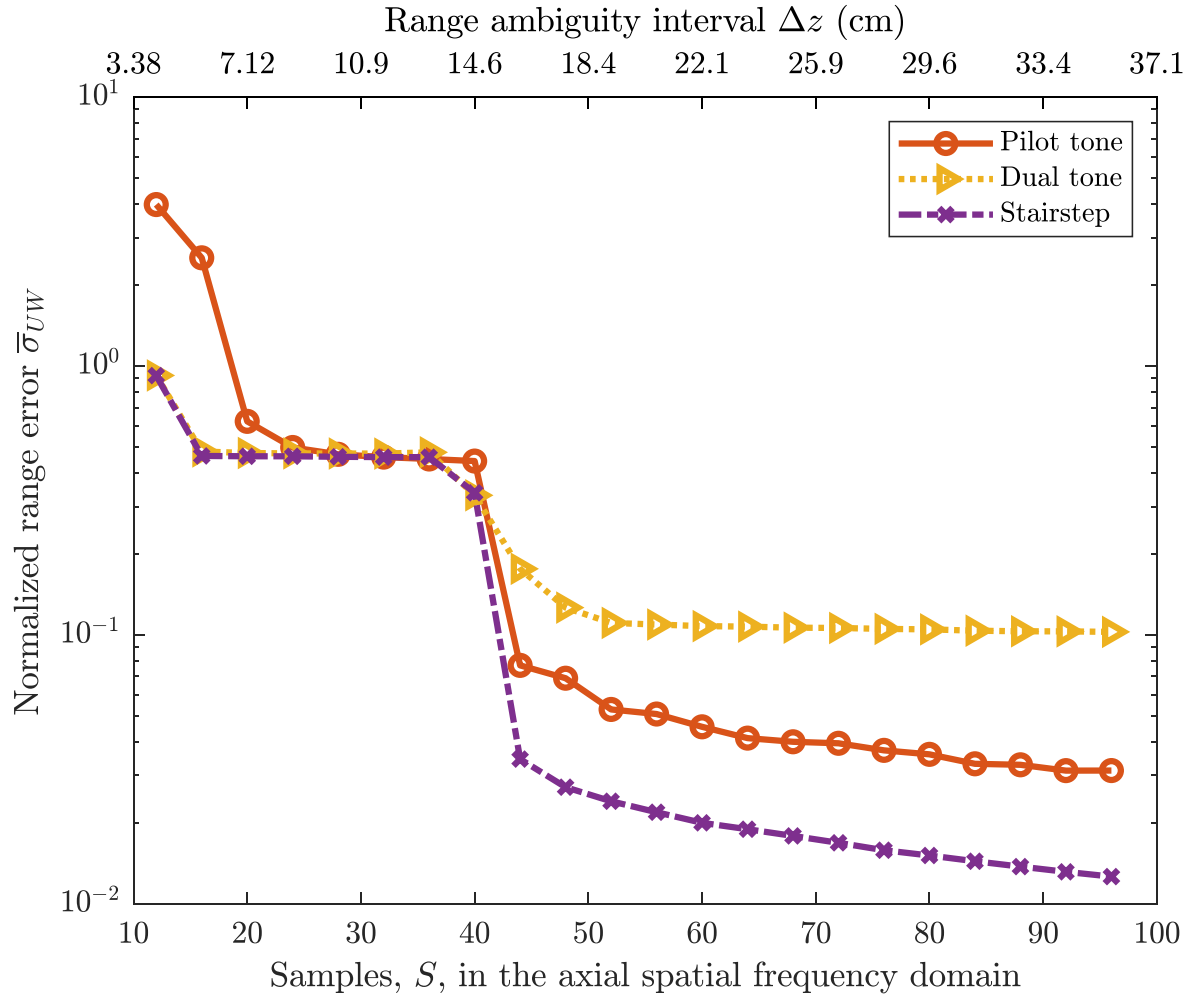




# Unwrapped range images: raised square plate



# Quantitative results for unwrapped range images



## Normalized Unwrapped Range Image Error

$$\bar{\sigma}_{UW} = \left( \text{std}_{u,v \in W(u,v)} \left[ \hat{R}(u,v) - R(u,v) \right] \right) / \Delta z$$

Range image
Truth range image

Recall max discontinuity of 8.5 cm

**Performance gets suddenly worse as  $\Delta z$  becomes less than twice the maximum range discontinuity**

Banet, M. T., Idris, A., & Fienup, J. R. (2023, October). Multiplexed, multi-wavelength 3D digital holographic imaging methods with range unwrapping. In *Unconventional Imaging, Sensing, and Adaptive Optics 2023* (Vol. 12693, pp. 12-24). SPIE.



# Signal-to-noise (SNR) model for pilot-tone and stairstep methods

## Pilot-tone 3D imaging

- We vary the SNR of each 2D coherent image,  $U(u, v; \nu)$ , with variable  $\text{SNR}_{U_n}$ .
- Each frequency-difference image is formed by a **single conjugate product operation** between images from the chirped illuminator and the pilot tone
- Phase noise from the two component images adds which reduces the effective SNR of each frequency difference image by a factor of  $\sqrt{2}$

$$E_n(u, v; \nu_n - \nu_p) = U_n U_{n,p}^*$$

$$\text{SNR}_{E_n} = \frac{\text{SNR}_{U_n}}{\sqrt{2}}$$

## Stairstep 3D imaging

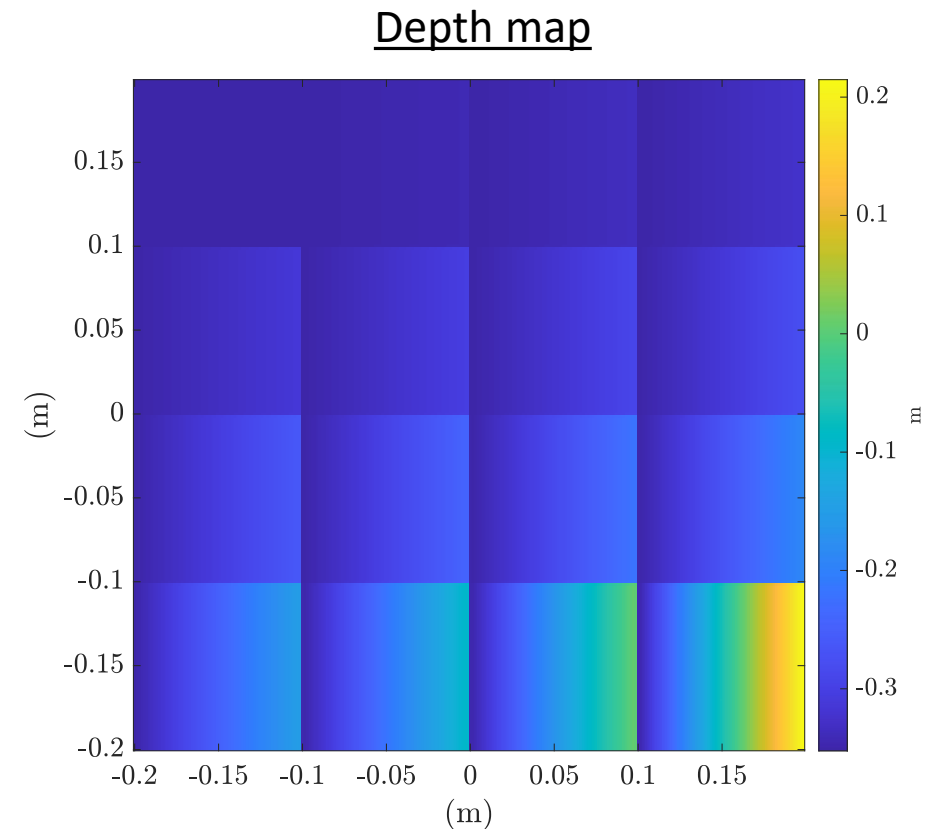
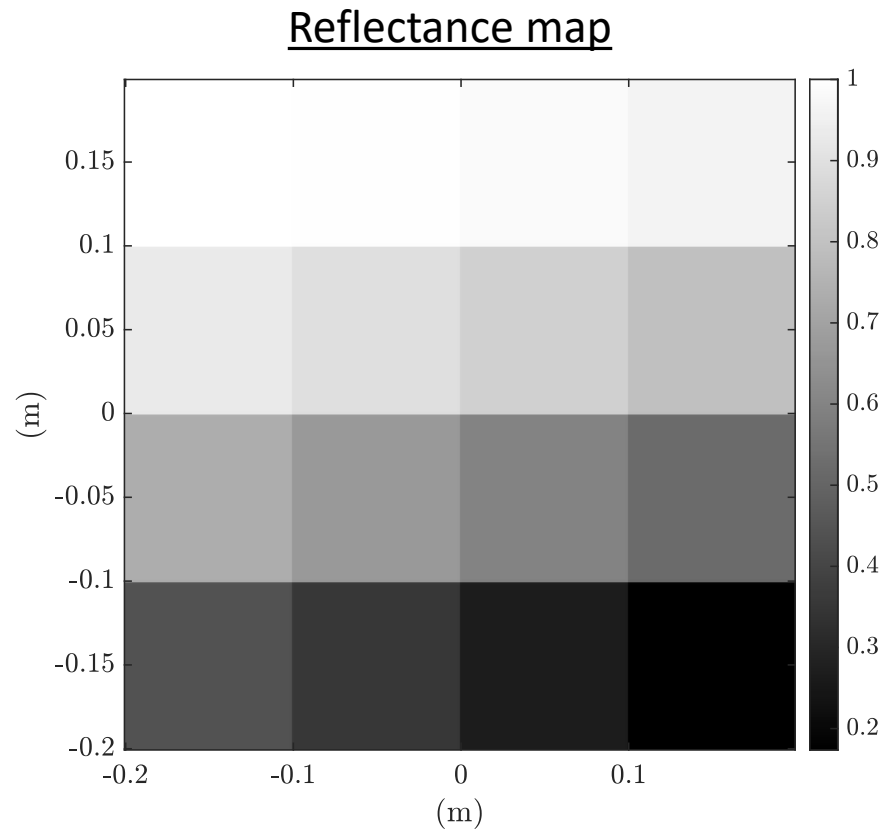
- We vary the SNR of each coherent image,  $U(u, v; \nu)$ , with variable  $\text{SNR}_{U_n}$ .
- Each frequency-difference image is formed by a **multiple conjugate product operations** that tie each coherent image to the master reference image
- Phase noise from the two component images adds which reduces the effective SNR of each frequency difference image by a factor of  $\sqrt{2n}$

$$E_n(u, v; \nu_n - \nu_{mr}) = U_n U_{n,br}^* \exp(i\angle E_{n-1})$$

$$\text{SNR}_{E_n} = \frac{\text{SNR}_{U_n}}{\sqrt{2n}}$$

# Simulation setup with picture of object

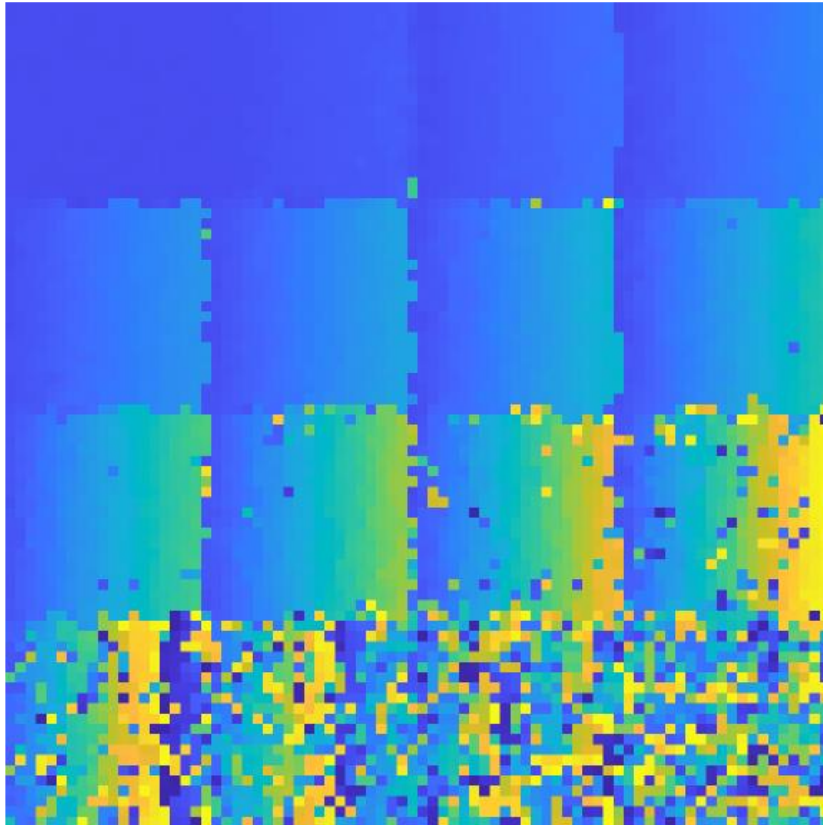
- Propagation distance,  $z = 2$  km
- Circular aperture diameter,  $D = 30$  cm
- Wavelength,  $\lambda = 1.5$   $\mu\text{m}$
- Varied # of samples in frequency difference space,  $P$
- Varied SNR of each 2D coherent image
- Kept total bandwidth  $\nu_{max} - \nu_{min}$  constant



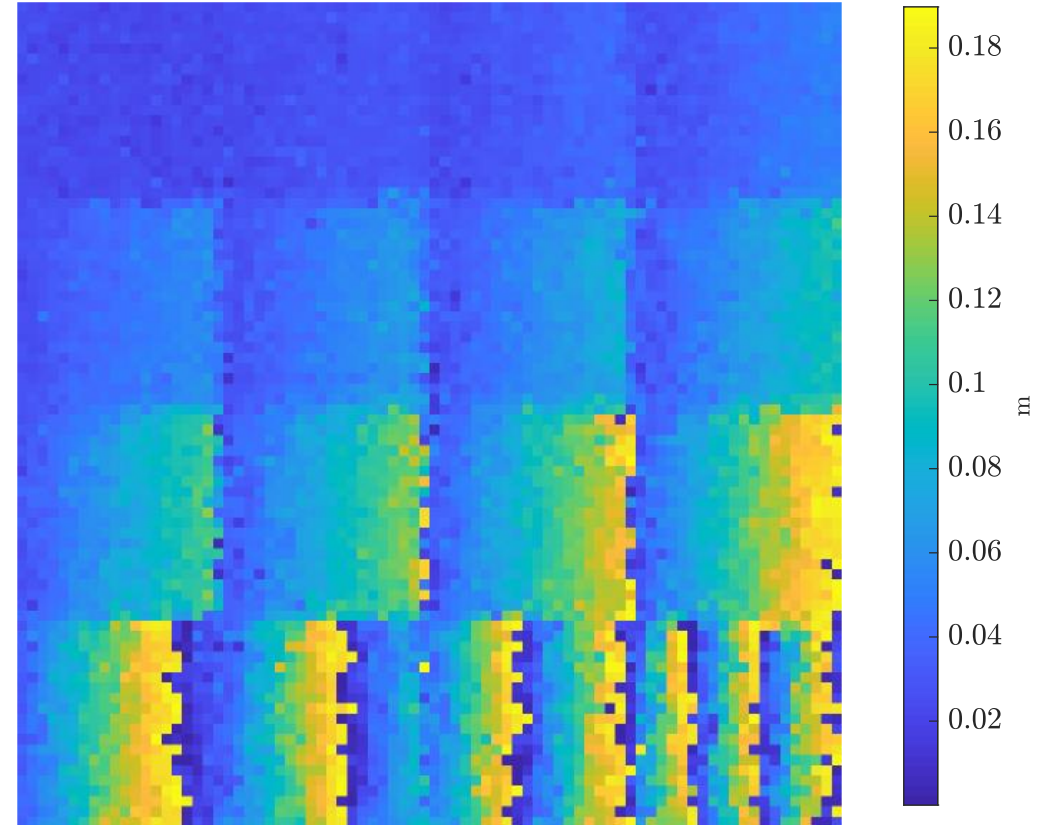


# Results: Range images for $P = 20$ and $\text{SNR}_{U_n} = 10$

Pilot tone range image

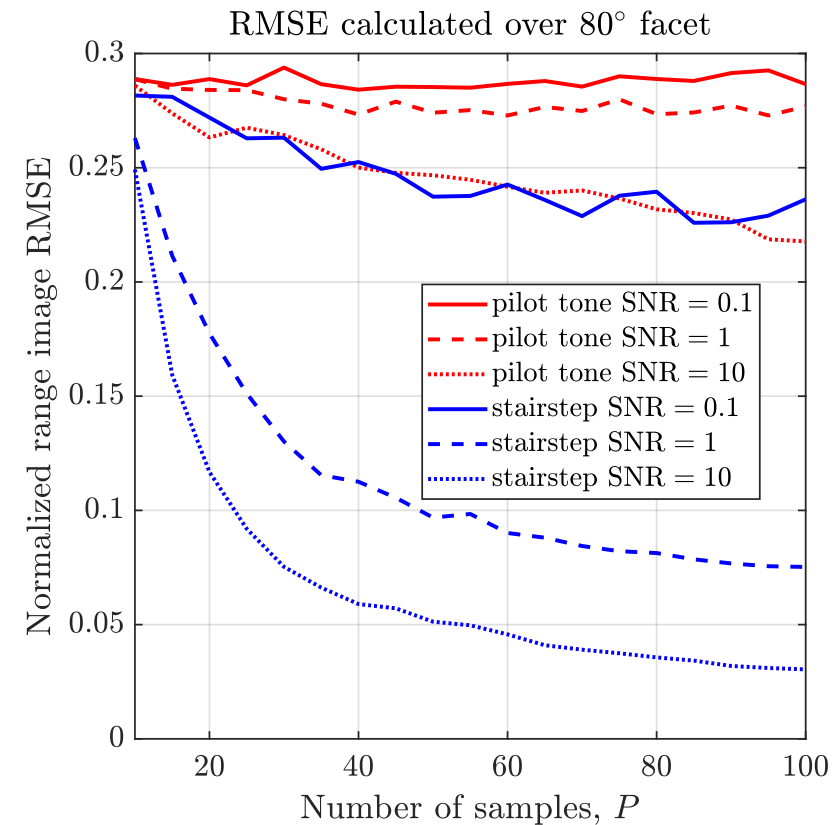
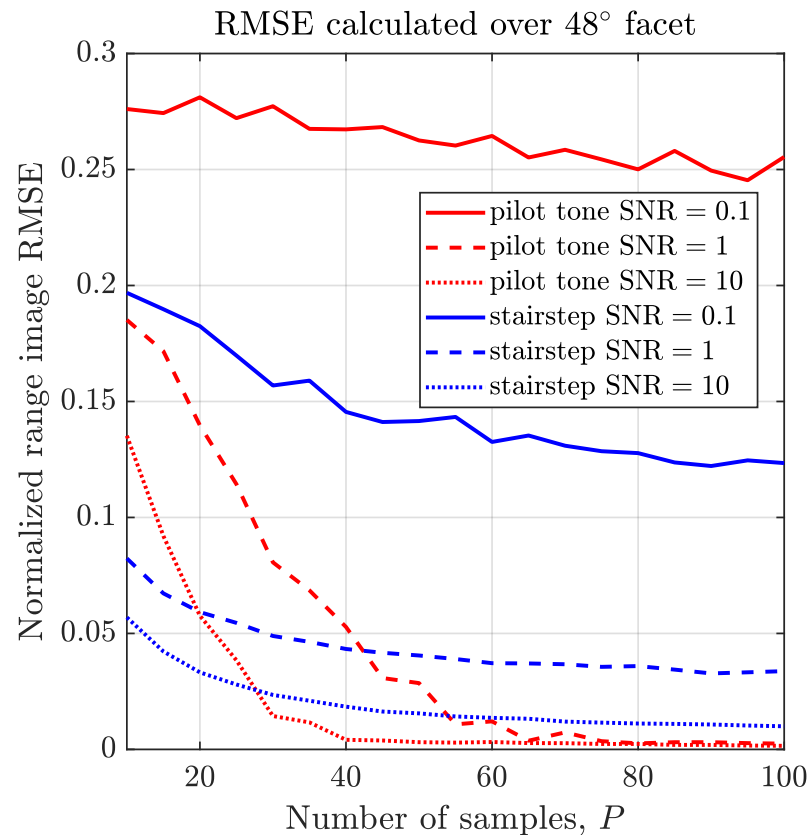
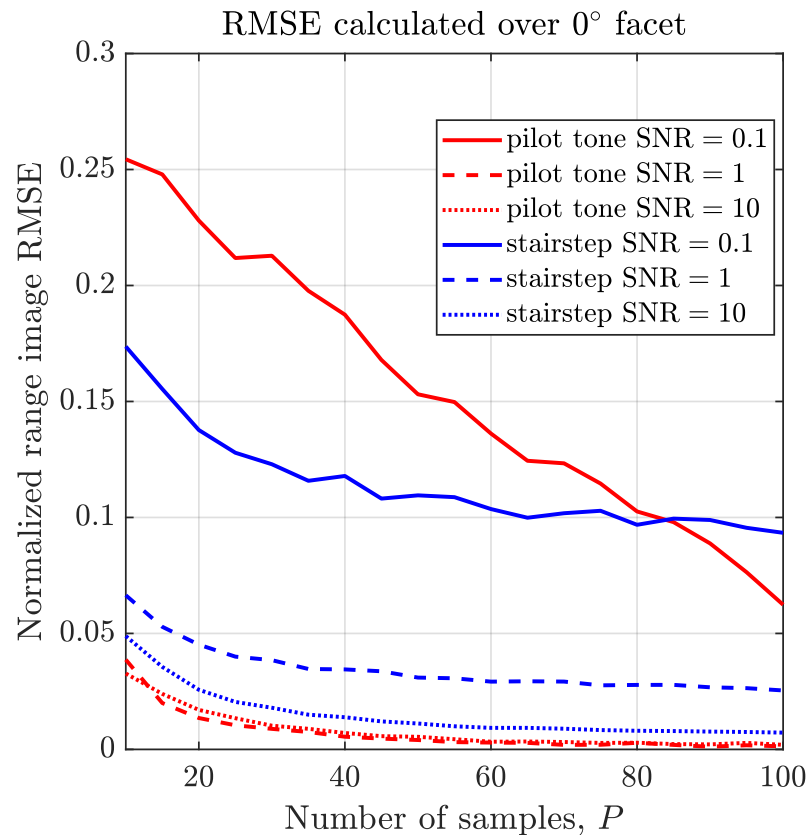


Stairstep range image





# Results: Range image root-mean-square error (RMSE) vs. $P$ for three different facet angles and various SNRs

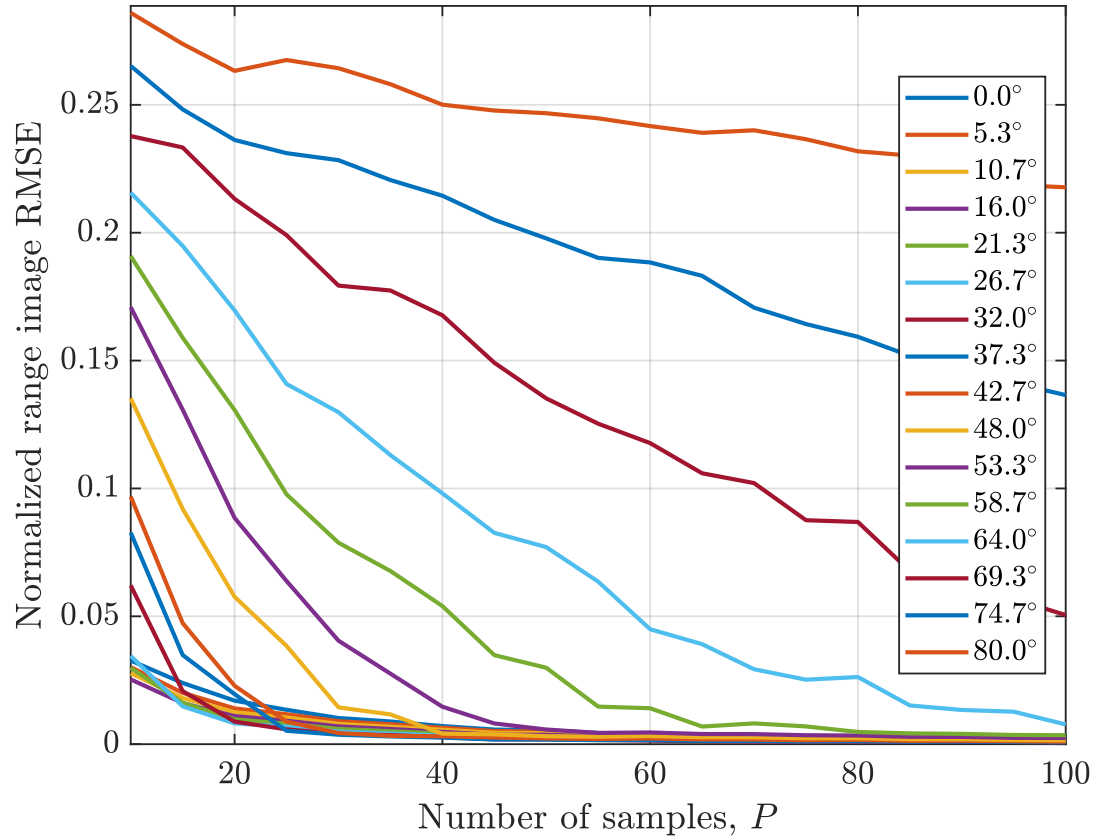


Banet, M. T., Wong, F., & Fienup, J. R. (2024, July). Stairstep versus pilot-tone 3D imaging: empirical signal-to-noise ratio studies. In Computational Optical Sensing and Imaging (pp. CF4A-2). Optica Publishing Group.

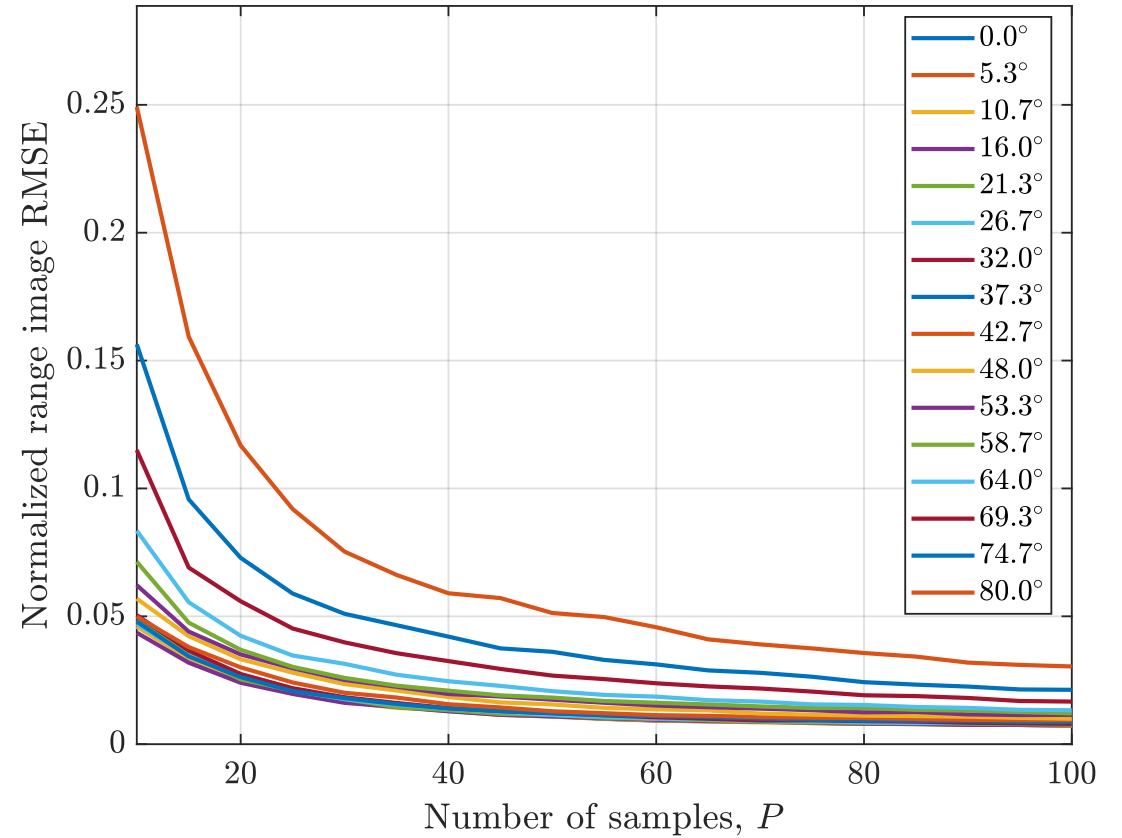


# Results: Range image RMSE vs. $P$ for three different facet angles and $\text{SNR}_{U_n} = 10$

Pilot-tone 3D imaging, SNR = 10



Stairstep 3D imaging, SNR = 10

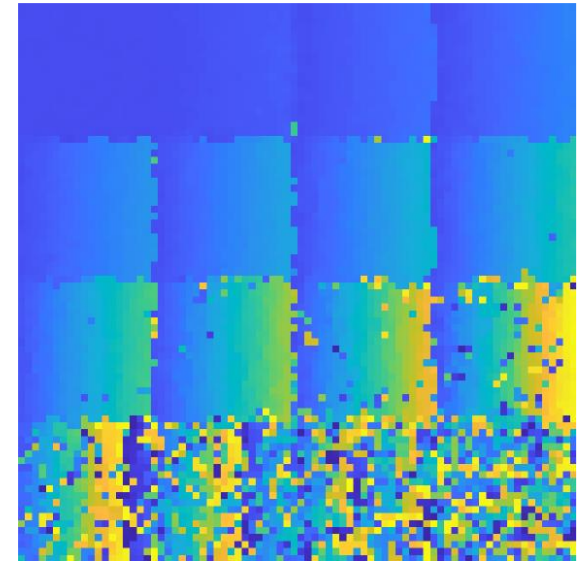


Banet, M. T., Wong, F., & Fienup, J. R. (2024, July). Stairstep versus pilot-tone 3D imaging: empirical signal-to-noise ratio studies. In Computational Optical Sensing and Imaging (pp. CF4A-2). Optica Publishing Group.

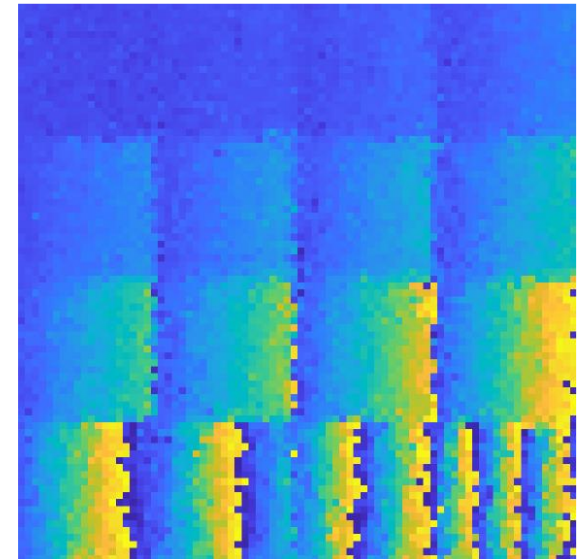
## Conclusions

- Stairstep imaging provides better results for highly sloped facets of the object
- Pilot tone imaging generally outperforms stairstep imaging for objects with shallow slopes and practical SNRs (1-10)
- Range unwrapping is viable when range discontinuities are less than half the range ambiguity interval
- Adding illuminators adds enables more modalities for motion-compensated 3D imaging

Pilot tone range image



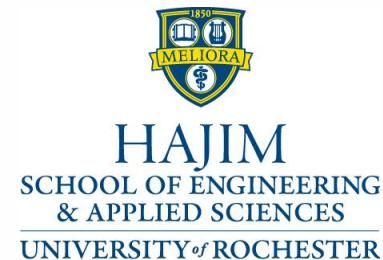
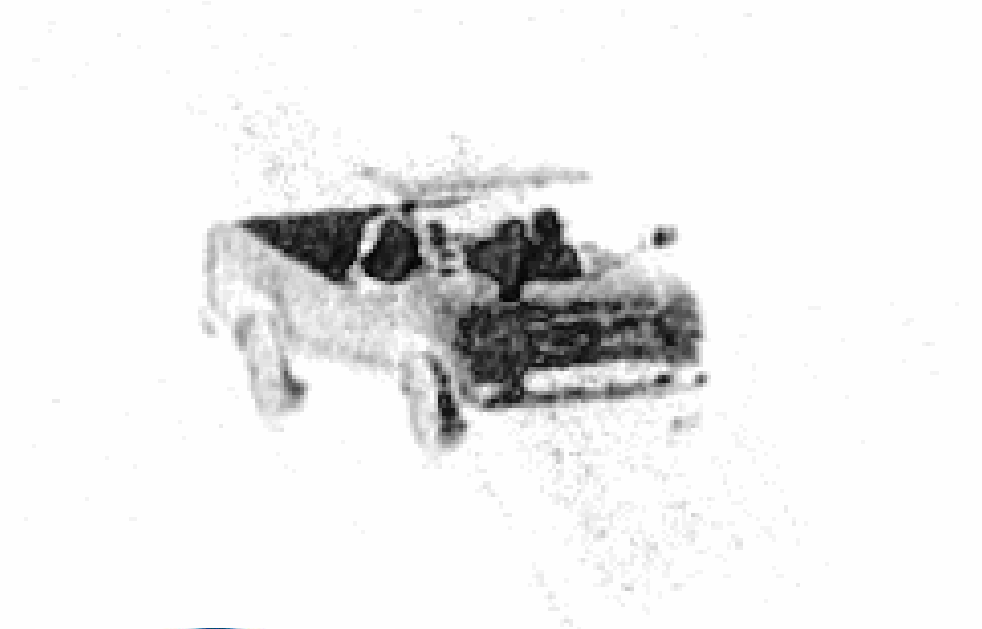
Stairstep range image





## Future work

- Exploring a hybrid approach that can leverage the best qualities of both methods
- Fleshing out the theoretical SNR models for each method for more in-depth comparisons
- Exploring alternate methods to dual-tone imaging that might perform well for moving/vibrating objects
- **Researchers at MZA Associates Corporation and Dr. Fienup's group at the University of Rochester are continuing this work!**

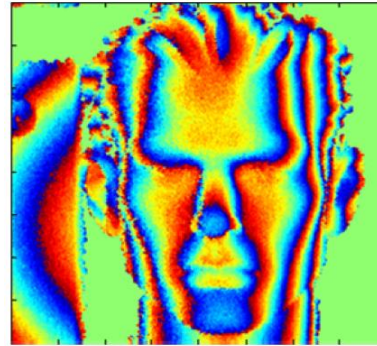


# Related work

- Phase difference imaging requires just two laser pulses of differing frequency (related to conjugate product images)
- 3D imaging with digital holography also enables 3D image reconstruction via sharpness metric maximization

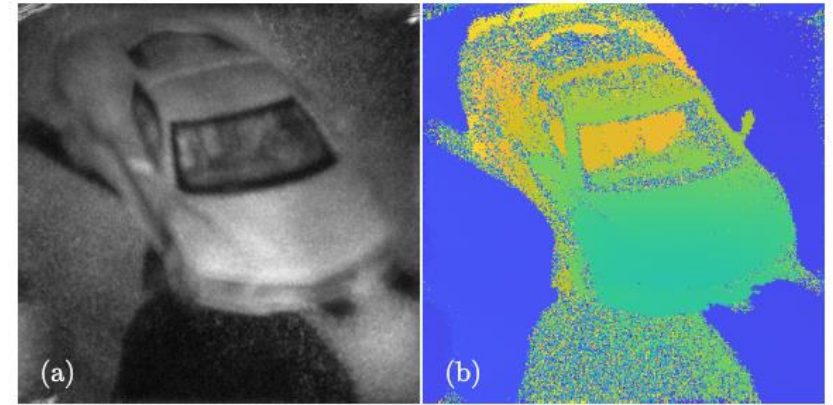
**Questions?**

Phase difference imaging<sup>1</sup>

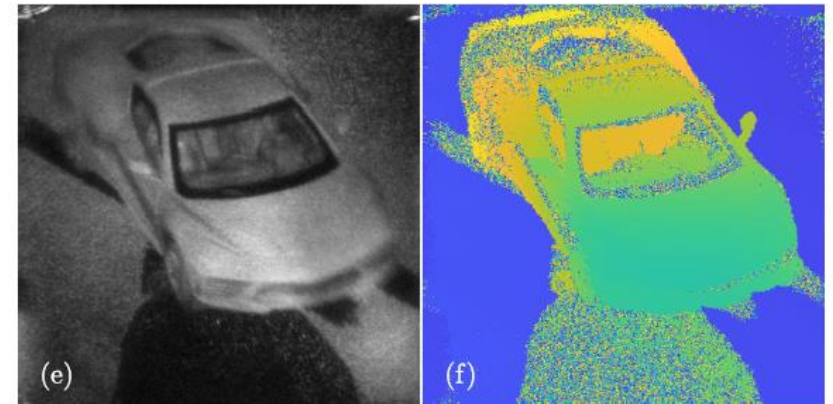


Motion-compensated 3D imaging<sup>2</sup>

Aberrated



Multi-plane



1. Marron, J. C., Kendrick, R. L., Thurman, S. T., Seldomridge, N. L., Grow, T. D., Embry, C. W., & Bratcher, A. T. (2010, April). Extended-range digital holographic imaging. In *Laser Radar Technology and Applications XV* (Vol. 7684, pp. 493-498). SPIE.
2. Banet, M. T., Fienup, J. R., & Krause, B. W. (2024). Demonstration of multi-plane sharpness metric maximization on motion-compensated, multi-wavelength 3D digital holographic field data. *Optics Letters*, 49(3), 418-421.

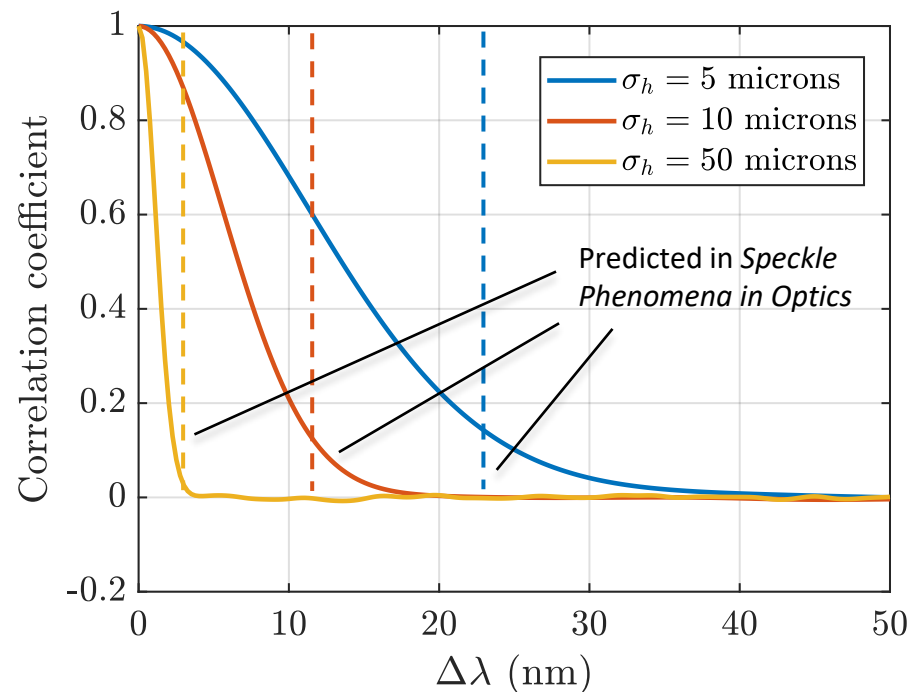


# Extra slides

# Speckle correlation with variable wavelength

- Assume that transverse correlation of surface roughness profile is delta-correlated (safe to assume for most wave-optics grid sample sizes)
- Isolate speckle decorrelation effects due to **surface roughness**, neglecting decorrelation effects from diffraction, which can be modeled easily

Irradiance correlation versus  $\Delta\lambda$  for  $\bar{\lambda} = 1 \mu\text{m}$



Reflective Samples	Enhancement ( $\eta$ )	Roughness ( $R_{\text{rms}}$ )
Brushed aluminum	122.3	1.5 $\mu\text{m}$
Infragold <sup>®</sup>	89.9	9.4 $\mu\text{m}$
Sandblasted aluminum	67.7	2.3 $\mu\text{m}$
Graphite	37.3	3.5 $\mu\text{m}$
White paint	36.8	1.7 $\mu\text{m}$
Spectralon <sup>®</sup>	13.8	Unprofiled
Transmissive Sample		
White paint	56.4	1.7 $\mu\text{m}$

Burgi, K., Ullom, J., Marciniak, M., & Oxley, M. (2016). Reflective inverse diffusion. Applied Sciences, 6(12), 370.

$$|\Delta\lambda| \geq \frac{1}{2\sqrt{2}\pi} \frac{\bar{\lambda}^2}{\sigma_h}$$

$1/e^2$  decorrelation point according to Eq. (6.47)  
(*Speckle Phenomena in Optics: Theory and Applications*, 2<sup>nd</sup> Ed.)





# Practical implications of speckle correlation with variable wavelength

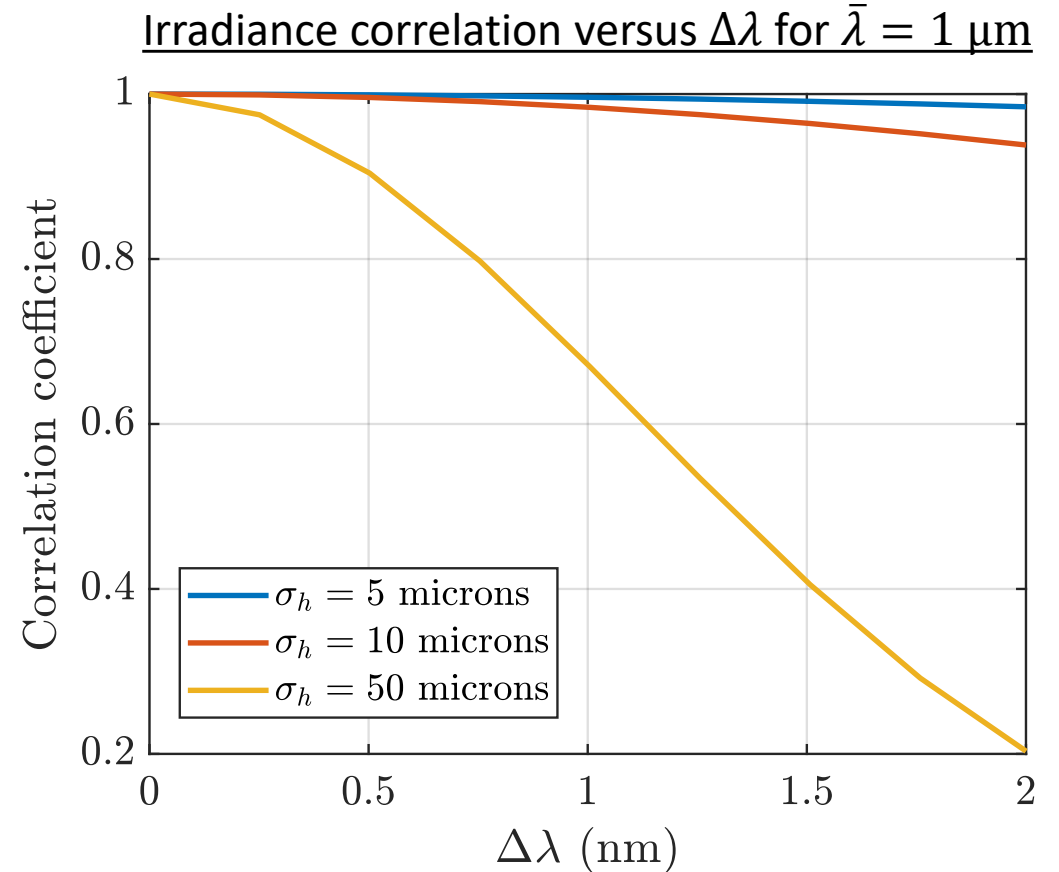
- Most modeling involves quasi-monochromatic light or **narrow fractional bandwidths** for which **surface roughness effects** are mostly unchanging
  - Long range 3D imaging:  $\Delta\nu \sim 30$  GHz or  $\Delta\lambda \sim 0.1$  nm at  $\bar{\lambda} = 1$   $\mu\text{m}$
- For narrow fractional bandwidths, object plane modeling can include a **coarse depth phasor** for diffractive effects and **circular complex Gaussian random numbers** for surface roughness effects

$$U_{1,\perp}(x, y) \exp[i2kZ_d(x, y)] [\mathcal{N}(0, 0.5) + i\mathcal{N}(0, 0.5)]$$

Models object reflectance

Models diffractive effects

Models surface roughness



Fractional bandwidth:  $\Delta\lambda/\bar{\lambda}$